

Application of Monod and Finite Element Models for Groundwater Cleanup in the Niger Delta Area of Nigeria

Chinike Okogbule-Wonodi¹, Uku Philip Eruni², Ekperi Nelson Ibezim³

Abstract

The Niger Delta region of Nigeria, recognized for its rich biodiversity and intensive oil and gas exploration, is increasingly threatened by environmental degradation, particularly groundwater contamination. This contamination poses significant risks to water resources, ecosystem stability, and public health. Addressing these challenges requires innovative remediation strategies. This study explores the application of Monod kinetics and Finite Element Models (FEM) to mitigate groundwater contamination in the Niger Delta. Monod kinetics is employed to evaluate microbial degradation rates in contaminated aquifers, offering insights into the biodegradation of hydrocarbons and other pollutants. The integration of FEM enables the simulation of groundwater flow and contaminant transport, providing a dynamic understanding of the interaction between pollutants and aquifers under varying environmental conditions. Together, these methodologies offer a dual approach: the Monod model predicts microbial activity essential for natural attenuation processes, while FEM identifies contaminant distribution and informs the design of efficient remediation systems. The study demonstrates that combining Monod kinetics and FEM allows for a more comprehensive assessment of contamination dynamics and provides targeted solutions for site-specific remediation. The results highlight the potential of this integrated approach to enhance the efficiency of groundwater cleanup efforts, reduce environmental risks, and promote sustainable management of water resources.

Keywords: Niger delta, groundwater contamination, Monod model, finite element model, environmental remediation, microbial degradation, groundwater flow

INTRODUCTION

The Niger Delta region, located in southern Nigeria, is an ecological hotspot and a major oil-producing area in Africa. However, decades of oil spills, gas flaring, and industrial waste disposal have severely impacted the environment, particularly the groundwater systems. Groundwater in this region is often contaminated with petroleum hydrocarbons, heavy metals, and other hazardous substances that threaten human health and the surrounding ecosystems [1-4].

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Efficient cleanup methods are necessary to restore the quality of groundwater and prevent further degradation. Among the various approaches, the integration of microbial degradation models and numerical groundwater flow simulations offers a promising strategy. This research explores the application of two key models—Monod kinetics and Finite Element Modeling (FEM)—for the management and remediation of contaminated groundwater in the Niger Delta.

METHODOLOGY

Groundwater Contamination in the Niger Delta

The Niger Delta is a critical water source for millions of people who rely on it for drinking, agriculture, and industrial use. The region's porous geology, consisting of alluvial deposits and unconsolidated sediments, makes it susceptible to contamination from surface activities. Oil spills from pipelines and offshore drilling platforms, illegal oil bunkering, and industrial waste disposal have led to the infiltration of harmful substances like hydrocarbons, heavy metals, and salinity into groundwater.

Research indicates that petroleum-derived contaminants such as benzene, toluene, ethylbenzene, and xylene (BTEX), as well as polycyclic aromatic hydrocarbons (PAHs), are frequently found in groundwater samples in the region. These pollutants not only degrade water quality but also pose serious health risks, including cancer, liver damage, and respiratory issues. Thus, the need for effective groundwater cleanup techniques is urgent.

Monod Model for Microbial Degradation

The Monod model is widely used to describe the growth of microorganisms and their interactions with pollutants in environmental systems. The model is based on the assumption that microbial growth is dependent on the availability of a limiting substrate (in this case, contaminants), [5] and it follows a Michaelis-Menten type kinetics.

The general form of the Monod equation is:

$$\mu = \mu_{\max} \frac{S}{K_s + S}$$

Where:

- μ is the specific growth rate of the microorganisms (per unit time),
- μ_{\max} is the maximum growth rate,
- S is the concentration of the contaminant (substrate),
- K_s is the half-saturation constant (the concentration of substrate at which the growth rate is half of the maximum).

In groundwater cleanup applications, the Monod model can be used to predict the rate at which microorganisms degrade contaminants over time. This model is particularly useful in bioremediation processes, where indigenous or added microbial populations are employed to degrade hydrocarbons and other organic pollutants.

For the Niger Delta, Monod kinetics can be applied to assess the potential of bioremediation using native bacteria or genetically engineered microorganisms capable of degrading petroleum hydrocarbons. The efficiency of these microbes in removing contaminants is influenced by environmental factors such as temperature, pH, and nutrient availability, all of which can be incorporated into the model for more accurate predictions.

Finite Element Model for Groundwater Flow and Contaminant Transport

Groundwater flow and contaminant transport are complex processes that are governed by various physical, chemical, and biological factors. Numerical models, such as the Finite Element Model (FEM), are widely used to simulate these processes and predict the movement and concentration of contaminants over time [6].

The FEM divides the study area into smaller elements, and the governing equations of flow and transport are solved for each element using numerical techniques. The key equations that FEM solves in groundwater modeling include:

Darcy's Law for groundwater flow:

$$\vec{Q} = -K\nabla h$$

Where:

\vec{Q} is the Darcy velocity (groundwater flow rate),
 K is the hydraulic conductivity,
 ∇h is the gradient of the hydraulic head.

By solving these equations, the FEM can simulate the movement of contaminants through the groundwater system, taking into account factors such as aquifer heterogeneity, boundary conditions, and sources of contamination.

In the context of groundwater cleanup in the Niger Delta, FEM can be used to simulate different remediation scenarios, such as pump-and-treat systems, bioremediation, and natural attenuation. The model helps to predict the long-term fate of contaminants and assess the effectiveness of various cleanup strategies.

Integration of Monod and FEM for Groundwater Cleanup [7-10]

The integration of Monod kinetics with FEM offers a powerful tool for simulating the microbial degradation of contaminants in groundwater. By coupling the Monod model's biological degradation rate with the transport equations of FEM, it becomes possible to predict both the spatial and temporal distribution of contaminants and microbial populations.

In the Niger Delta, this coupled model can be used to:

- *Evaluate Bioremediation Feasibility:* By simulating the degradation rates of different contaminants in various aquifers, the model can help determine the optimal conditions (such as nutrient concentration, temperature, and microbial population density) for bioremediation in specific contaminated zones.
- *Optimize Cleanup Strategies:* The FEM can be used to simulate different intervention methods, such as the injection of nutrients to stimulate microbial growth or the use of bioreactors to enhance degradation. This helps in identifying the most cost-effective and efficient cleanup strategies.
- *Assess Long-term Effects:* The integrated model can simulate the long-term dynamics of groundwater quality, providing insights into how contaminants will behave over time and how quickly they will be removed through natural attenuation or bioremediation.

Model Expansion

Expanding the equation

$$\partial R(w, \tau) = \frac{\partial R}{\partial w} \partial w + \frac{\partial R}{\partial \tau} \partial \tau = 0 \quad (1)$$

$$\frac{\partial R}{\partial w} = K_T, \frac{\partial R}{\partial \tau} = -P \quad (2)$$

$$\partial a = 2\Delta w \partial w + 2\Delta \tau (\phi P)^2 \partial \tau = 0$$

$$\partial R = R_n - R_0, \partial a = a_n - a_0 \quad (3)$$

where n and $n =$ new and old value

$$\begin{bmatrix} R_0 \\ a_0 \end{bmatrix} = \begin{bmatrix} K_T & -P \\ 2\Delta w & 2\Delta \tau (\phi P)^2 \end{bmatrix} \begin{bmatrix} \partial w \\ \partial \tau \end{bmatrix} \quad (4)$$

Again

$$\frac{\partial R}{\partial W} = K \frac{d^2 R}{dw^2} - P \frac{dw}{d\tau} \quad (5)$$

By Galerkin Finite Element Formulation method

$$R(\tau) = W_i^e R_{ci} + W_{i+1}^e R_{ci+1} = [W][R_c] \quad (6)$$

$$\int_0^t W^T \left(K \frac{\partial^2 R_c}{\partial W^2} - P \frac{\partial R_c}{\partial w} - \frac{\partial W}{\partial \tau} \right) d\tau = 0 \quad (7)$$

Equation 3 can further be evaluated into:

$$\int_0^t W^T K \frac{\partial^2 R_c}{\partial W^2} d\tau = \int_0^t \frac{\partial W}{\partial \tau} \frac{\partial}{\partial \tau} [W] [R] d\tau = 0 \quad (8)$$

$$= \frac{K}{\tau} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} R_1 \\ R_2 \end{bmatrix} \quad (9)$$

Again 2nd term evaluation

$$\int_0^t W^T K \frac{\partial R_c}{\partial w} dw = \int_0^t W^T K \frac{\partial}{\partial \tau} [W] [R] d\tau = 0 \quad (10)$$

$$= \frac{K}{2} \begin{bmatrix} 1 & 1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} R_1 \\ R_2 \end{bmatrix} \quad (11)$$

3rd term Evaluation

$$\int_0^t W^T \frac{\partial R_c}{\partial \tau} d\tau \quad (12)$$

$$= \frac{\tau}{6} \begin{bmatrix} 2 & 1 \\ -1 & 2 \end{bmatrix} \begin{bmatrix} R_1 \\ R_2 \end{bmatrix} \quad (13)$$

$$\frac{K}{\tau} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} R_1 \\ R_2 \end{bmatrix} - \frac{K}{2} \begin{bmatrix} 1 & 1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} R_1 \\ R_2 \end{bmatrix} + \frac{\tau}{6} \begin{bmatrix} 2 & 1 \\ -1 & 2 \end{bmatrix} \begin{bmatrix} R_1 \\ R_2 \end{bmatrix} \quad (14)$$

Considering that $K_1 = \frac{K}{\tau}$ and $\frac{K}{2}$

$$\begin{bmatrix} K_1 + K_2 & -K_1 - K_2 & 0 & 0 & 0 \\ -K_1 + K_2 & 2K_1 & -K_1 - K_2 & 0 & 0 \\ 0 & -K_1 + K_2 & 2K_1 & -K_1 + K_2 & 0 \\ 0 & 0 & -K_1 + K_2 & 2K_1 & -K_1 - K_2 \\ 0 & 0 & 0 & -K_1 + K_2 & K_1 - K_2 \end{bmatrix} \begin{bmatrix} R_1 \\ R_2 \\ R_3 \\ R_4 \\ R_5 \end{bmatrix} = 0 \quad (13)$$

RESULTS AND DISCUSSION

Discussions

From Figure 1 to 3, the plot reveals that the conductivity of fresh water increased linearly where there was a reduction in the conductivity of underground water. There was a high degree of rapid reduction in the conductivity of fresh water. The pH value also decreased linearly tending to be more acidic due to contamination or either crude oil or metal in it, whereas the pH value of underground and fresh water first increase during the first week and the gradually decreased to acidic value.

Table 1. Evaluated physiochemical properties of underground water.

| Underground Water | | | |
|-------------------|--------------|------|-----------------------------|
| | Conductivity | pH | Temperature 0 ^{oc} |
| Initial Reading | 0.61 | 6.2 | 26.60 |
| Week 1 | 0.39 | 5.85 | 25.6 |
| Week 2 | 0.35 | 5.70 | 26.2 |
| Week 3 | 0.31 | 5.76 | 27.0 |
| Week 4 | 0.25 | 5.69 | 26.1 |
| Week 5 | 0.20 | 5.60 | 25.5 |
| Week 6 | 0.19 | 5.50 | 24.4 |
| Week 7 | 0.18 | 5.45 | 22.2 |
| Week 8 | 0.15 | 5.30 | 23.02 |

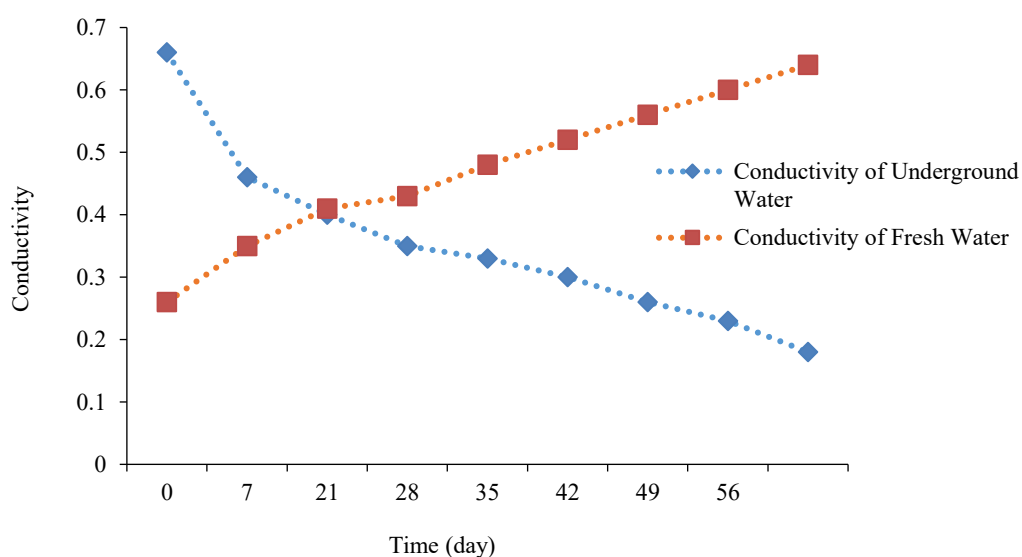


Figure 1. Conductivity versus time for underground water and fresh water environment.

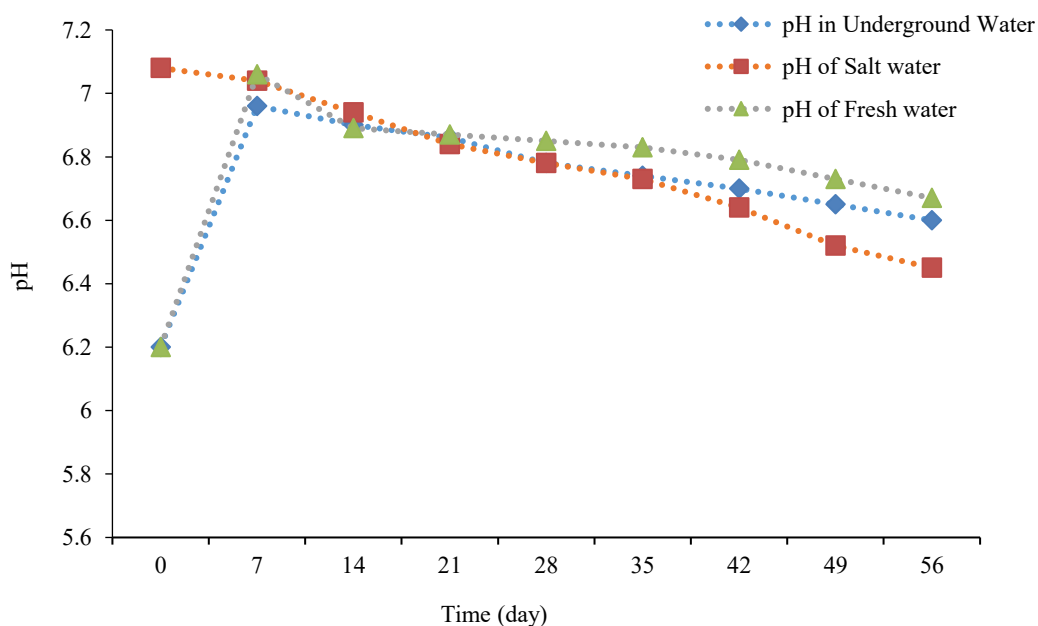


Figure 2. Comparison of pH versus time in Underground for Salt and fresh water environment.

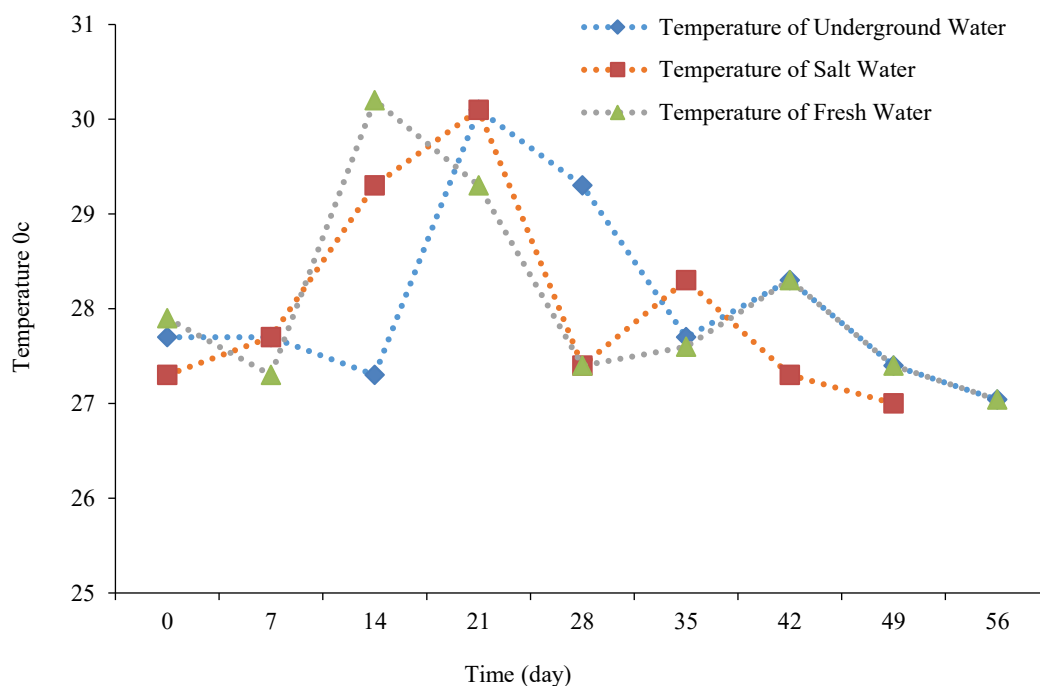


Figure 3. Comparison of temperature versus time in underground, salt and fresh water environment.

CONCLUSION

The application of Monod and Finite Element Models in groundwater cleanup provides a robust and integrated approach to managing contamination in the Niger Delta. By combining microbial degradation kinetics with advanced numerical simulations of groundwater flow and contaminant transport, it is possible to design effective remediation strategies tailored to the unique conditions of the region. This approach not only improves the efficiency of groundwater cleanup but also offers valuable insights for the sustainable management of water resources in oil-impacted areas.

The research underscores the importance of combining biological and physical models for environmental cleanup, paving the way for more effective strategies to restore groundwater quality in the Niger Delta and similar regions worldwide.

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