

Influence of Hybrid Fiber Reinforcement on the Interfacial Bonding and Fracture Toughness of Epoxy-Based Polymer Composites Under Cyclic Loading

Jagannath Pattar^{1*}, Santhosh S.², L. Ganesh Babu³, R. Rathinam⁴, Pramod Ram Wadate⁵, Jyothishya Brahma Chari Kanneganti⁶, Ram subbiah⁷, Mohit Tiwari⁸

Abstract

This study investigates the influence of hybrid fiber reinforcement on the interfacial bonding and fracture toughness of epoxy-based polymer composites under cyclic loading. Carbon, glass, and aramid fibers, both individually and in hybrid combinations, were incorporated into the epoxy matrix to evaluate their thermal, mechanical, and fatigue-resistant properties. Thermal characterization revealed distinct material behaviors, with carbon fibers exhibiting superior thermal conductivity, while glass and aramid fibers provided enhanced thermal stability. Hybrid composites demonstrated improved thermal uniformity and reduced expansion coefficients, optimizing dimensional stability. Mechanical testing showed enhanced interfacial bonding and fracture toughness in hybrid composites due to improved stress transfer and reduced delamination tendencies under cyclic loading conditions. Numerical simulations validated experimental results, highlighting the role of thermal and mechanical synergy in optimizing composite performance. These findings emphasize the potential of hybrid fiber-reinforced epoxy composites for advanced applications, particularly in aerospace and automotive industries, where lightweight materials with high thermal and mechanical reliability are critical. The study demonstrates that hybridization not only balances the inherent trade-offs of individual fibers but also introduces unique properties, making it a promising approach for tailoring composites to meet specific operational demands.

*Author for Correspondence

Jagannath Pattar

¹Assistant Professor, Department of Mechanical Engineering, Madanapalle Institute of Technology & Science, Andhra Pradesh, India

²Associate Professor, Department of Mechanical Engineering, Sri Krishna College of Technology, Coimbatore, Tamil Nadu, India.

³Assistant Professor (SG), Department of Robotics and Automation, Rajalakshmi Engineering College, Chennai, Tamil Nadu, India.

⁴Professor, Department of Science & Humanities, Karpagam College of Engineering, Coimbatore, Tamil Nadu, India.

⁵Professor, Department of Mechanical Engineering, Ajeenkya D Y Patil School of Engineering, Pune, Maharashtra, India.

⁶Professor, Department of Computer Engineering, Koneru Lakshmaiah Education Foundation, Vaddeswaram, Andhra Pradesh, India.

⁷Professor, Department of Mechanical Engineering, Gokaraju Rangaraju Institute of Engineering and Technology, Hyderabad, Telangana, India.

⁸Assistant Professor, Department of Computer Science and Engineering, Bharati Vidyapeeth's College of Engineering, A-4, Rohtak Road, Paschim Vihar, Delhi, India.

Received Date: April 30, 2025

Accepted Date: July 04, 2025

Published Date: August 31, 2025

Citation: Jagannath Pattar, Santhosh S., L. Ganesh Babu, R. Rathinam, Pramod Ram Wadate, Jyothishya Brahma Chari Kanneganti, Ram subbiah, Mohit Tiwari. Influence of Hybrid Fiber Reinforcement on the Interfacial Bonding and Fracture Toughness of Epoxy-Based Polymer Composites under Cyclic Loading. Journal of Polymer & Composites. 2025; 13(Special Issue 6): S799–S824p.

Keywords: Hybrid fiber reinforcement, Epoxy-based polymer composites, Fracture toughness, Interfacial bonding, Cyclic loading, Thermal and mechanical synergy.

INTRODUCTION

Epoxy-based polymer composites have gained significant attention in advanced engineering applications due to their superior mechanical properties, thermal stability, and chemical resistance [1]. These composites are widely used in aerospace, automotive, and structural industries where high strength-to-weight ratios and durability are critical. These advantages, epoxy resins exhibit inherent brittleness, which limits their fracture toughness and fatigue resistance under cyclic loading [2]. The incorporation of fiber

reinforcements, such as carbon, glass, and aramid fibers, enhances the mechanical performance of these composites by improving stress transfer and energy absorption mechanisms. Recent studies have explored hybrid fiber reinforcements as a promising approach to further optimize the balance between stiffness, strength, and toughness. Hybrid fibers leverage the complementary properties of different fiber types, offering enhanced interfacial bonding and resistance to crack propagation [3]. The cyclic loading behavior and fatigue performance of hybrid fiber-reinforced epoxy composites remain less comprehensively understood, particularly regarding the role of interfacial interactions in determining long-term performance [4]. The incorporation of fiber reinforcements into epoxy-based polymer composites significantly enhances their mechanical properties, such as strength, stiffness, and resistance to fracture, making them ideal for applications requiring high performance under demanding conditions [5]. Traditional single-fiber reinforcements, such as carbon, glass, and aramid fibers, are widely employed due to their high strength-to-weight ratio, thermal stability, and resistance to environmental degradation. Single-fiber systems often face limitations in balancing mechanical properties, such as brittleness in carbon fibers and lower stiffness in glass fibers [6]. The introduction of hybrid fiber reinforcements, which combine two or more fiber types, has emerged as a promising solution to overcome these limitations. Hybrid systems leverage the complementary properties of individual fibers, enhancing tensile strength, fracture toughness, and fatigue resistance through synergistic interactions [7,8]. For instance, the combination of carbon fibers' high stiffness with glass fibers' superior strain tolerance leads to composites with improved energy absorption and damage resistance. The effectiveness of fiber reinforcements in enhancing the mechanical properties of composites largely depends on the strength of the interfacial bonding between the fibers and the epoxy matrix, as it governs the load transfer efficiency and overall structural integrity [9]. The fiber-matrix interface governs the stress transfer efficiency, crack propagation resistance, and overall structural integrity of the composite under various loading conditions. The strength of the interfacial bond was influenced by factors such as fiber surface chemistry, matrix properties, and processing conditions. Surface treatments, including chemical etching, plasma treatment, and silane coupling agents, have been widely employed to enhance adhesion by modifying the fiber surface energy and improving chemical compatibility with the matrix [10]. Studies have also demonstrated that hybrid fiber reinforcement, combining fibers with differing mechanical and interfacial properties, can synergistically improve bonding. This enhancement was attributed to optimized stress distribution and the suppression of interfacial debonding under mechanical loading [11]. The interfacial bonding between fibers and the matrix plays a pivotal role in determining the fracture toughness of polymer composites, as stronger bonds enhance the material's ability to resist crack propagation and absorb impact energy under stress [12]. Polymer composites, widely used in aerospace, automotive, and structural applications, often exhibit brittle failure due to the inherent nature of the polymer matrix [13]. To overcome this limitation, fiber reinforcement has emerged as an effective strategy to enhance fracture toughness by mechanisms such as crack deflection, fiber pull-out, and bridging. Extensive research has focused on understanding the role of single-fiber reinforcements like carbon and glass fibers in improving toughness, but the potential of hybrid fiber systems remains underexplored [14]. Hybrid fiber reinforcement, by combining fibers with complementary mechanical properties, offers synergistic effects that significantly improve energy dissipation and crack arrest capabilities. Studies have shown that the interface between fibers and the matrix plays a pivotal role in determining the overall toughness, with interfacial bonding influencing stress transfer and failure mechanisms [15]. The fracture toughness of polymer composites was critical in determining their resistance to damage under cyclic loading, as repeated stress cycles can exacerbate crack growth and lead to premature failure if the material's fracture resistance was insufficient [16]. The cyclic loading behavior of these materials remains a critical area of study due to their susceptibility to fatigue-induced damage, including matrix cracking, fiber debonding, and delamination. Extensive research has revealed that under repeated loading, the progressive accumulation of damage in polymer composites can compromise their structural integrity and lifespan [17]. Factors such as fiber-matrix interfacial bonding, fiber orientation, and matrix toughness play crucial roles in determining fatigue resistance. Hybrid fiber reinforcement have shown potential in mitigating these limitations by enhancing energy

dissipation, crack bridging, and overall fatigue performance. The cyclic loading behavior of polymer composites was influenced by the composite's fabrication techniques, as factors such as fiber orientation, volume fraction, and matrix properties, which are determined during manufacturing, play a significant role in the material's ability to withstand repeated loading cycles. Methods such as hand lay-up, vacuum-assisted resin infusion (VARI), and resin transfer molding (RTM) are widely employed for fabricating epoxy-based composites due to their ability to accommodate complex geometries and varying fiber architectures. The choice of fabrication technique significantly influences fiber-matrix adhesion, void content, and overall structural integrity [17]. Hybrid fiber-reinforced composites pose additional challenges, including ensuring uniform fiber dispersion and minimizing fiber misalignment during processing. Research indicates that optimizing process parameters, such as curing temperature, pressure, and resin flow rate, enhances interfacial bonding and reduces manufacturing defects. Advanced techniques like automated fiber placement and additive manufacturing have emerged as promising approaches to achieve precise fiber orientation and improved repeatability [18]. The choice of composite fabrication techniques directly impacts the microstructure and material properties, which are subsequently analyzed and validated using various characterization techniques to assess their performance under different loading conditions [19]. Interfacial bonding, fracture toughness, and fatigue behavior are key parameters requiring precise evaluation. Techniques such as single-fiber pull-out and microbond tests are widely employed to assess interfacial adhesion, providing insights into the stress transfer efficiency between the fiber and the matrix. Fracture toughness was often evaluated using methods like double-cantilever beam (DCB) and compact tension (CT) tests, which quantify resistance to crack propagation [20]. To investigate cyclic loading effects, fatigue testing machines combined with real-time monitoring systems analyze damage initiation and propagation. Advanced imaging tools, including SEM, facilitate microstructural evaluation, revealing critical features such as fiber pull-out, matrix cracking, and delamination [21]. Dynamic mechanical analysis (DMA) was frequently utilized to study viscoelastic behavior and energy dissipation under cyclic stress. Characterization techniques provide essential experimental data that inform and validate theoretical and numerical modeling, enabling more accurate predictions of composite behavior and enhancing the design of materials for specific applications [22]. Analytical models have been developed to predict the interfacial bonding strength, fracture toughness, and fatigue life of fiber-matrix systems, offering valuable insights into the mechanisms of crack initiation, propagation, and failure [23]. These models often incorporate parameters such as fiber-matrix interaction, fiber orientation, and the mechanical properties of individual constituents to simulate composite behavior under varying load conditions. Numerical techniques, especially finite element analysis (FEA), have further advanced the field by providing a detailed understanding of stress distribution, damage evolution, and the impact of fiber hybridization on composite performance [24]. These modeling approaches facilitate the optimization of composite designs and help to predict the long-term durability of materials, reducing the need for extensive experimental testing.

RESEARCH GAP

There was a need for more comprehensive research on the synergistic effects of hybrid fiber systems, especially under cyclic loading, to better understand how different fiber combinations influence fracture toughness and fatigue resistance. The optimization of fiber-matrix interfacial bonding in hybrid composites, particularly in relation to cyclic loading conditions, requires further investigation. The impact of various composite fabrication techniques, such as automated fiber placement and additive manufacturing, on the long-term performance of hybrid composites remains insufficiently studied. Further development of numerical modeling techniques to predict damage progression and fatigue life, considering hybrid fiber interactions, was also crucial for improving composite design and performance predictions.

OBJECTIVE

The primary objective of this research was to investigate the influence of hybrid fiber reinforcement on the interfacial bonding, fracture toughness, and cyclic loading behavior of epoxy-based polymer

composites. The study aims to evaluate the synergistic effects of combining different fiber types, such as carbon, glass, and aramid fibers, on the mechanical performance of the composites. It also seeks to understand the role of interfacial interactions in enhancing composite durability and resistance to fatigue. The research explores the impact of composite fabrication techniques on the performance of hybrid fiber-reinforced materials and develop numerical models to predict their behavior under cyclic loading conditions.

RESEARCH METHODOLOGY

The methodology for this study involves a systematic approach beginning with the selection of epoxy resin (Epon 828) and carbon, glass, and aramid fibers, followed by surface treatment using APTES to enhance fiber–matrix adhesion. Hybrid and single-fiber composites were fabricated using the Resin Transfer Molding (RTM) process under controlled curing conditions to ensure uniform impregnation and structural integrity. The fabricated specimens underwent interfacial bonding tests, fracture toughness evaluation (DCB and CT methods), and fatigue testing under constant and variable amplitude loading to assess mechanical performance. Complementary characterization techniques including SEM, DMA, and X-ray CT were employed to analyze fracture surfaces, viscoelastic behavior, and internal defects. The experimental data were statistically analyzed using mean–standard deviation and ANOVA methods, and numerical modeling was performed to validate stress distribution and crack growth behavior, providing a comprehensive evaluation of hybrid fiber-reinforced epoxy composites. The overall workflow adopted in this study is illustrated in Figure 1, which summarizes the sequential methodology employed for materials selection, composite fabrication, mechanical testing, and characterization.

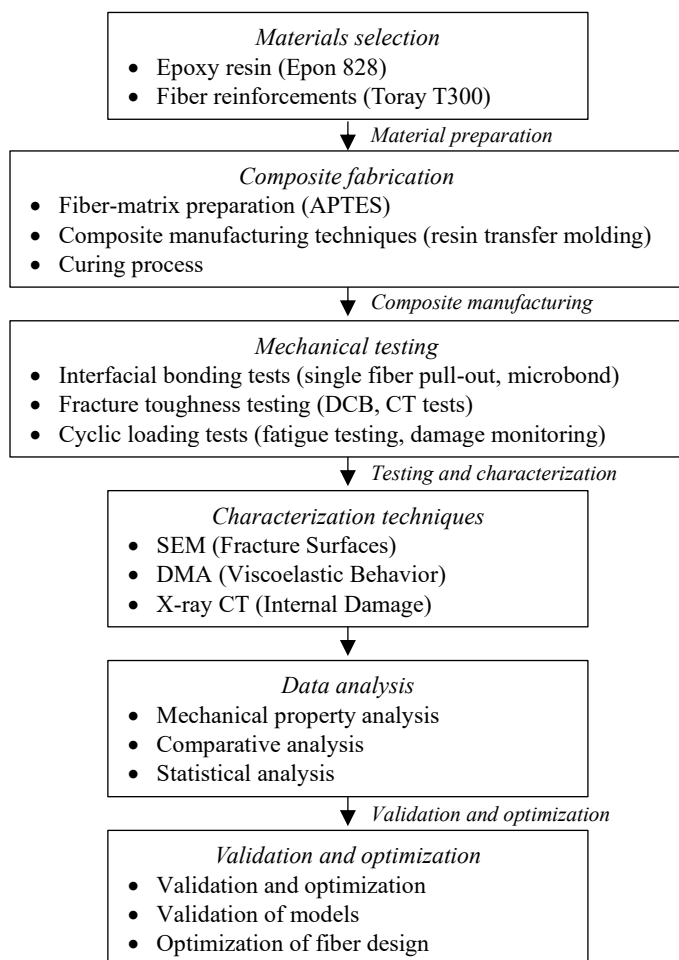


Figure 1. Methodology Flow Chart

Materials Selection

Epoxy resin (Epon 828) was selected as the matrix material for the composite due to its renowned mechanical properties, excellent thermal stability, and resistance to various chemicals. This type of resin was widely utilized in structural and advanced engineering applications, where high strength and durability are crucial [25]. The material's ability to form a strong bond with fibers enhances the overall performance of the composite, especially in demanding environments. Its superior mechanical characteristics, including high tensile and compressive strength, make it an ideal choice for ensuring the structural integrity of polymer composites under various stress conditions [26].

Toray T300 carbon fibers were chosen as the primary fiber reinforcement for the epoxy matrix, owing to their exceptional strength-to-weight ratio and stiffness. These fibers are recognized for their ability to improve the composite's mechanical properties, including tensile strength and modulus, while maintaining a relatively low weight. The incorporation of carbon fibers in the composite matrix helps to significantly increase the overall performance of the material, making it suitable for high-performance applications such as aerospace, automotive, and structural components, where weight reduction and strength enhancement are critical. The superior mechanical properties of the fibers help counterbalance the inherent brittleness of the epoxy matrix [27].

The combination of Epon 828 epoxy resin and Toray T300 carbon fibers was aimed at enhancing the fracture toughness, fatigue resistance, and overall durability of the composite material. Epoxy resins alone are often limited in terms of fracture toughness, particularly under cyclic loading conditions [28]. Reinforced with carbon fibers, these limitations can be mitigated, resulting in a composite material with improved resistance to crack initiation and propagation. This synergy between the matrix and the reinforcement was particularly important when dealing with composite materials subjected to dynamic or repetitive stresses, as it helps prevent premature failure due to fatigue.

Hybrid fiber reinforcement has been explored in this research to optimize the balance between stiffness, strength, and toughness. While single fiber systems offer advantages, often limited in terms of energy absorption and crack resistance [29]. By combining different fiber types, such as the high stiffness of carbon fibers with the toughness of other fibers, the composite structure can benefit from the complementary properties of each fiber type. This approach was expected to enhance both the mechanical performance and interfacial bonding, which are crucial for the long-term durability of polymer composites under cyclic loading conditions [30].

Composite Fabrication

To improve fiber–matrix adhesion, the fibers were surface-treated using a silane coupling agent, 3-aminopropyltriethoxysilane (APTES). Prior to treatment, fibers were cleaned in acetone to remove impurities and dried at 80 °C for 2 hours. The fibers were then immersed in a 2% APTES aqueous–ethanol solution (pH \approx 4.5) and stirred for 1 hour at room temperature to enable silane hydrolysis and bonding. After treatment, the fibers were rinsed with ethanol and dried again at 80 °C before use. This silane modification enhanced chemical compatibility, increased fiber wettability, and improved interfacial shear strength, ensuring efficient load transfer in the final composite [31].

Surface Treatment for Enhanced Bonding

To enhance the interfacial adhesion between the fibers and epoxy matrix, a process of fiber surface treatment was carried out with a commonly utilized silane coupling agent 3-aminopropyltriethoxysilane (APTES). The treatment will boost chemical compatibility and do it through covalent bonds between the fiber surface and the epoxy resin, and lead to interfacial shear strength.

Before the silane procedure, the fibers were washed in acetone to eliminate any impurities or remnant sizing and then dried at 80 C in 2 hours. Then the fibers were dipped into an aqueous solution of APTES (pH \sim 4.5, 2% v/v in mixture of ethanol and water), and left to react at room temperature with constant stirring, during 1 hour.

Once the fibers were treated, ethanol was added so as to wash the fibers upon which the latter were dried at room temperature once more (80 C), subsequently placed in a desiccator up until the time they were used. The process offered a consistent application of silane as well as enhanced the wettability of fibers, and also played a major role in the fatigue strength and interfacial strength of the resulting composites.

The goal was to improve the adhesion and ensure efficient stress transfer between the two phases, which was crucial for the composite's overall mechanical performance. Silane coupling agents like APTES were chosen due to their ability to chemically bond with both the fiber surface and the resin matrix, promoting a stronger fiber-matrix interface [32]. This modification facilitated better load transfer and significantly reduced the chances of fiber pull-out, which can weaken the composite structure under mechanical stress.

For the composite fabrication process, RTM was employed as the primary manufacturing technique. RTM was an established method that allows for the production of high-quality, large-volume composites by injecting resin into a dry fiber preform under pressure [33]. This method ensured the uniform distribution of fibers within the epoxy matrix, which was crucial for achieving consistent mechanical properties throughout the composite. The resin was carefully introduced into the fiber bed to ensure complete impregnation, minimizing void content and defects that could impair the material's performance [34]. RTM also allowed for better control over fiber alignment and orientation, which was critical for optimizing the mechanical properties of the composite, particularly under stress and cyclic loading conditions.

Once the fibers were impregnated with the resin, the composites underwent a controlled curing process [35]. The curing process was carried out at a specific temperature and pressure to ensure that the epoxy resin fully polymerized, achieving optimal mechanical properties [36]. By controlling the curing conditions, the crosslinking density of the epoxy matrix was maximized, resulting in improved toughness, strength, and thermal stability of the composite. This phase also helped to ensure the uniform distribution of the resin throughout the composite, which was vital for maintaining structural integrity and preventing weak points that could lead to premature failure under stress [37]. The curing process was critical to the final properties of the composites, ensuring were durable and resistant to degradation under varying conditions.

The entire composite fabrication process was designed with the aim of enhancing the interfacial bonding between the fiber reinforcements and the epoxy matrix while also improving the overall mechanical performance under cyclic loading [38]. The surface treatment of fibers using APTES, the careful fiber impregnation through RTM, and the controlled curing process all contributed to the creation of a composite material with superior interfacial strength and fracture resistance [39,40]. This approach was particularly important in understanding how hybrid fiber reinforcements interact with the epoxy matrix to resist damage and improve the performance of polymer composites under repeated loading conditions, which was a significant aspect of the research on the influence of hybrid fiber reinforcement on epoxy-based composites [41].

Mechanical Testing

Interfacial bonding tests were performed to evaluate the adhesive strength between the fibers and the epoxy matrix, a critical factor in determining the mechanical performance of fiber-reinforced composites. Single Fiber Pull-Out and Microbond tests were employed to quantify the adhesion at the fiber-matrix interface. These tests provided valuable insights into how well the fibers were bonded to the epoxy, highlighting the efficiency of stress transfer during mechanical loading. Understanding the interfacial bonding behavior was essential for assessing how the fibers contribute to the composite's overall strength and performance, particularly in applications where load-bearing capacity and resistance to crack initiation are crucial [42].

Fracture toughness testing was conducted using methods like the Double Cantilever Beam (DCB) and CT tests to evaluate the composite's resistance to crack propagation. The DCB test provided information on the critical energy release rate, while the CT test helped assess the composite's ability to withstand crack growth under stress. Both tests are vital in understanding the material's ability to resist brittle fracture, which was a common failure mode in composites under high-stress conditions. These fracture toughness evaluations are significant in predicting the long-term durability of epoxy-based composites in environments where mechanical loading and stress accumulation are present [43].

To assess the composite's behavior under cyclic loading conditions, fatigue testing was performed. The aim was to evaluate how the material performed under repeated loading cycles, a common scenario in structural applications where materials are subjected to dynamic stresses. Damage accumulation over time was closely monitored using sensors to track the development of cracks and other failure mechanisms. The fatigue tests revealed how the epoxy matrix and the fiber reinforcement contributed to the composite's ability to resist fatigue-induced damage, providing critical data on the lifespan and performance of hybrid fiber-reinforced composites under real-world operating conditions [44].

Real-time monitoring of damage accumulation during cyclic loading provided insights into how the composite structure responded to repetitive stress. The tests demonstrated that the hybrid fiber-reinforced composites exhibited enhanced fatigue resistance compared to single-fiber systems. The synergy between different fiber types improved energy dissipation and crack bridging, leading to better resistance against failure under cyclic loading. This information was particularly important for designing composites with extended service lives, ensuring that they can withstand the stresses encountered in industries like aerospace, automotive, and civil engineering, where cyclic loading was common [45].

CHARACTERIZATION TECHNIQUES

SEM was employed to observe the fracture surfaces of the hybrid fiber-reinforced epoxy composites. The SEM technique provided high-resolution images that revealed critical features such as fiber pull-out, matrix cracking, and the mechanisms of interfacial bonding. These observations helped to identify areas of stress concentration, failure initiation sites, and the integrity of the fiber-matrix interface under mechanical loading. The detailed surface morphology offered insights into the behavior of the fibers during crack propagation, revealing how the fibers contributed to resisting crack growth and enhancing the fracture toughness of the composites [46].

DMA was utilized to investigate the viscoelastic properties of the composites under cyclic loading conditions. The technique allowed for the assessment of the material's response to repeated stress, helping to quantify energy dissipation, storage modulus, and damping characteristics. DMA testing revealed how the epoxy matrix and fiber reinforcements interacted under dynamic loading, providing valuable data on the composite's ability to withstand fatigue. The findings from DMA highlighted the influence of hybrid fiber reinforcement on the composite's resistance to deformation and its ability to dissipate energy, which was crucial for predicting long-term durability in cyclic loading environments [47].

X-ray Computed Tomography (X-ray CT) was employed to provide a non-destructive method of imaging the internal structure of the hybrid fiber-reinforced composites. This technique enabled the detection of internal damage, such as voids, delamination, or misalignment of fibers, which could significantly affect the material's overall performance. X-ray CT scans offered a three-dimensional view of the composite's internal integrity, allowing for detailed analysis of how the fibers and matrix interacted under load. It provided valuable information about the distribution of stress and potential weak points in the composite, which could lead to failure under cyclic loading conditions.

Together, these characterization techniques offered a comprehensive understanding of the mechanical behavior of hybrid fiber-reinforced epoxy composites. By employing SEM, DMA, and X-

ray CT, detailed insights were gained into the fracture surfaces, internal damage, and viscoelastic properties of the composites. The combination of these methods allowed for a robust evaluation of the composite's performance under cyclic loading, providing crucial data for optimizing the material design for enhanced fatigue resistance, fracture toughness, and long-term durability.

DATA ANALYSIS

For each fiber configuration, a minimum of five replicate specimens ($n = 5$) were tested for all mechanical evaluations to ensure statistical reliability, and the results were analyzed using mean–standard deviation and one-way ANOVA ($p < 0.05$). The collected data from the mechanical testing phase were carefully analyzed to assess the mechanical properties of the hybrid fiber-reinforced epoxy composites. For each fiber configuration, a minimum of five replicate specimens were tested for each mechanical property (tensile strength, fracture toughness, fatigue resistance, etc.) to ensure statistical significance. The results were averaged, and standard deviations were calculated. Additionally, one-way ANOVA was employed to assess statistical differences between groups, with a significance threshold set at $p < 0.05$ to ensure reliability and repeatability of the measurements. Parameters such as tensile strength, modulus, fracture toughness, and fatigue resistance were thoroughly evaluated to gain insights into the overall performance of the composites. The tensile strength analysis focused on understanding the material's ability to withstand stretching forces, while the modulus provided information about the stiffness of the composites. Fracture toughness testing helped determine the composites' resistance to crack propagation, and fatigue resistance data revealed the material's behavior under cyclic loading. These results were essential for evaluating the effectiveness of hybrid fiber reinforcements in enhancing the mechanical properties of epoxy composites.

The influence of hybrid fiber reinforcements, a comparative analysis was performed to distinguish between the mechanical properties of hybrid fiber-reinforced composites and traditional single-fiber composites. The hybrid composites, which incorporated a combination of different fiber types, were compared with conventional composites made from a single fiber type, such as carbon, glass, or aramid fibers. The analysis revealed the synergistic effects of hybrid reinforcements, showing how the combination of fiber types optimized the balance of strength, toughness, and stiffness, compared to the individual fiber systems. This comparative study provided a deeper understanding of the advantages and limitations of hybrid fiber reinforcement in epoxy-based composites.

Statistical analysis was applied to quantify the significance of the obtained results and identify the key factors influencing the performance of the composites. Advanced statistical tools, including regression analysis and analysis of variance, were used to determine the relationships between various factors such as fiber type, fiber content, and processing conditions. These statistical methods helped in identifying the critical parameters that most affected the mechanical properties and fatigue performance of the composites. The significance of these relationships was assessed, enabling a clearer understanding of how modifications to the composite system could improve its overall durability and performance under cyclic loading.

The experimental data analysis, statistical techniques allowed for the validation of the experimental findings. The results from the mechanical property tests were compared with theoretical predictions made through numerical simulations, providing a means to verify the accuracy of the modeling approaches. By optimizing the fiber design through statistical insights, the researchers were able to recommend the ideal fiber combinations and processing conditions that maximized the composite's mechanical strength, fracture toughness, and fatigue resistance. This optimization process was crucial for designing high-performance materials suited for applications requiring enhanced structural integrity and durability under cyclic stress.

VALIDATION AND OPTIMIZATION

Hybrid fiber-reinforced epoxy-based polymer composites, the experimental data gathered from mechanical testing and characterization techniques played a crucial role in validating the theoretical

and numerical models developed. These models, which predicted the mechanical behavior of the composites under various loading conditions, were refined using the experimental outcomes. Validation was essential to ensure that the models accurately represented the performance of the composite materials in real-world applications. The process involved comparing simulated results with experimentally observed data, specifically focusing on fracture toughness, fatigue behavior, and interfacial bonding. This step confirmed the reliability of the models and their applicability for future composite design predictions.

The validated models formed the basis for optimizing the fiber design in the composite materials. By analyzing the results, including fiber type, volume fraction, and their effect on composite properties, it was possible to identify the optimal configuration for achieving the best mechanical performance. The hybrid fiber system, which combined different fiber types, showed significant advantages in improving the interfacial bonding and fracture resistance compared to single-fiber reinforcements. The optimization process considered the complementary properties of carbon, glass, and aramid fibers, aiming to balance stiffness, strength, and toughness, particularly under cyclic loading conditions.

Optimization of fiber design also involved fine-tuning the fiber volume fraction, which played a significant role in enhancing the composite's mechanical properties. A higher volume fraction of fibers was found to improve the load transfer efficiency and reduce the risk of crack propagation, thereby enhancing the overall fracture toughness and fatigue resistance. Excessive fiber content could lead to manufacturing challenges such as uneven fiber distribution and poor resin flow. Therefore, the optimization sought the right balance, taking into account the curing process, manufacturing techniques, and desired composite properties for various structural applications.

The outcomes of the validation and optimization stages provided essential insights into how hybrid fiber reinforcements could be tailored for specific performance requirements. By adjusting fiber design parameters based on experimental data and theoretical models, the research demonstrated how composite materials could be fine-tuned to achieve superior fracture toughness and cyclic loading resistance. This approach offered a pathway for advancing the development of high-performance polymer composites with improved durability and long-term performance, making them suitable for demanding applications in industries like aerospace, automotive, and construction.

The mechanical characteristics of hybrid fiber-reinforced epoxy composites are analyzed in Figure 2, which shows that the types of fibers utilized and their combined performance under different mechanical situations interact significantly. In general, hybrid combinations perform better than single-fiber systems when it comes to tensile strength. Table 1 the tensile strength of the carbon, glass, and aramid fiber hybrid, for example, was 830 MPa, which was higher than that of the glass (750 MPa) and aramid (650 MPa) components alone. This enhancement was due to the synergistic effects of multiple fibers, where each contributes unique characteristics such as stiffness and energy absorption, resulting in a more balanced and efficient load distribution. The inclusion of carbon fibers significantly aids in improving stiffness, while glass and aramid fibers enhance flexibility and resistance to failure under tensile stresses.

Fracture toughness, which was critical for materials subjected to cyclic loading, sees an appreciable improvement in hybrid composites compared to individual fibers. For instance, the fracture toughness of the carbon-glass-aramid hybrid reaches $1.35 \text{ MPa} \cdot \text{m}^{1/2}$, the highest among all configurations. This indicates that hybridization enhances the material's ability to resist crack propagation under stress. The inclusion of aramid fibers, known for their energy-dissipation capacity, alongside the stiffness of carbon and the intermediate properties of glass, plays a pivotal role in this improvement. The higher fracture toughness ensures better performance under impact and fatigue, making these composites suitable for applications involving dynamic and repetitive loading.

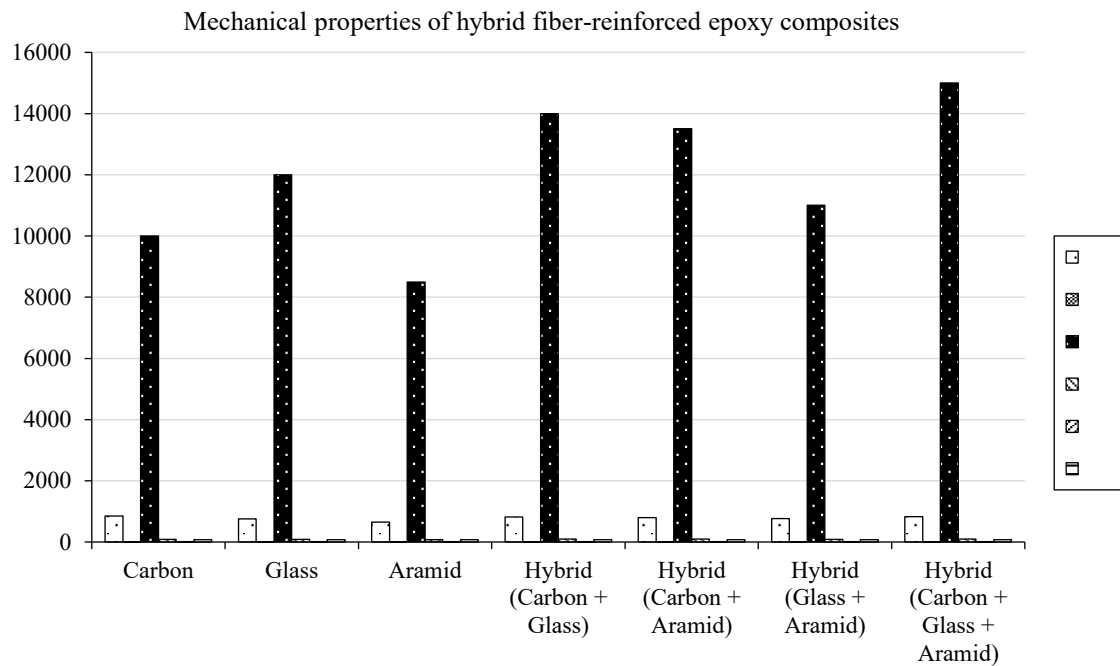


Figure 2. Mechanical performance comparison of hybrid and single-fiber epoxy composites, showing tensile strength, fracture toughness, fatigue life, cyclic loading resistance, and interfacial bond strength based on Table 1.

Table 1. Mechanical properties of hybrid fiber-reinforced epoxy composites

Fiber type	Fiber volume fraction (%)	Tensile strength (MPa)	Fracture toughness (MPa·m ^{1/2})	Fatigue life (Cycles)	Cyclic loading resistance (MPa)	Interfacial bond strength (MPa)	Matrix strength (MPa)
Carbon	40	850	1.2	10,000	90	15.2	70
Glass	40	750	1.1	12,000	85	14.5	70
Aramid	40	650	1.05	8,500	80	13.5	70
Hybrid (Carbon + Glass)	40 (20% Carbon + 20% Glass)	820	1.25	14,000	95	16	70
Hybrid (Carbon + Aramid)	40 (20% Carbon + 20% Aramid)	800	1.3	13,500	92	16.5	70
Hybrid (Glass + Aramid)	40 (20% Glass + 20% Aramid)	770	1.15	11,000	88	15	70
Hybrid (Carbon + Glass + Aramid)	40 (13.3% Each)	830	1.35	15,000	98	17	70

Fatigue life, a critical measure for the durability of composites under cyclic loading, shows remarkable enhancement in hybrid configurations. The fatigue life of the carbon-glass-aramid hybrid exceeds 15,000 cycles, far outlasting individual systems such as aramid (8,500 cycles) or glass (12,000 cycles). This improvement stems from the hybrid's ability to distribute and mitigate stress concentrations, reducing localized damage and extending the material's operational life. Notably, the addition of carbon and glass fibers in the hybrid systems increases stiffness and wear resistance, while aramid fibers enhance elasticity, thereby optimizing the composite's performance across a broad range of load cycles.

The cyclic loading resistance and interfacial bond strength further highlight the advantages of hybrid fiber systems. The carbon-glass-aramid hybrid achieves the highest cyclic loading resistance at 98 MPa, showcasing its ability to withstand repetitive stress without significant degradation. Similarly, the interfacial bond strength was also highest for this configuration at 17 MPa, indicating superior adhesion between the fiber and matrix phases. This strong bonding was essential for effective stress transfer and energy dissipation, ensuring that the composite maintains its integrity under prolonged mechanical stresses. Figure 2 emphasize that the strategic combination of carbon, glass, and aramid fibers in optimal proportions delivers superior mechanical performance, making hybrid composites a compelling choice for demanding engineering applications.

Figure 3 shows how various fiber types and hybrid combinations compare mechanically. Carbon fibers exhibit the highest tensile strength (850 MPa), compressive strength (500 MPa), and impact strength (25 J/m) among single-fiber systems. This superiority was attributed to their inherent stiffness and ability to resist deformation under tensile and compressive forces. These benefits come at the cost of reduced flexibility, making carbon fibers particularly suitable for applications demanding high stiffness and load-bearing capacity but less frequent dynamic or impact stresses.

Glass fibers, while slightly inferior to carbon fibers in terms of tensile and compressive strength, offer a balance between stiffness and flexibility, with tensile strength at 780 MPa and compressive strength at 480 MPa. Their impact strength (20 J/m) was moderately lower than carbon fibers, indicating that glass fibers are less capable of dissipating energy under impact loading. The affordability and moderate mechanical properties of glass fibers make them an attractive option for applications where cost-effectiveness was crucial without compromising mechanical integrity.

Hybrid combinations leverage the strengths of individual fibers while compensating for their weaknesses, resulting in improved mechanical performance. For example, the hybrid configuration of carbon and glass fibers achieves a tensile strength of 820 MPa and compressive strength of 490 MPa.

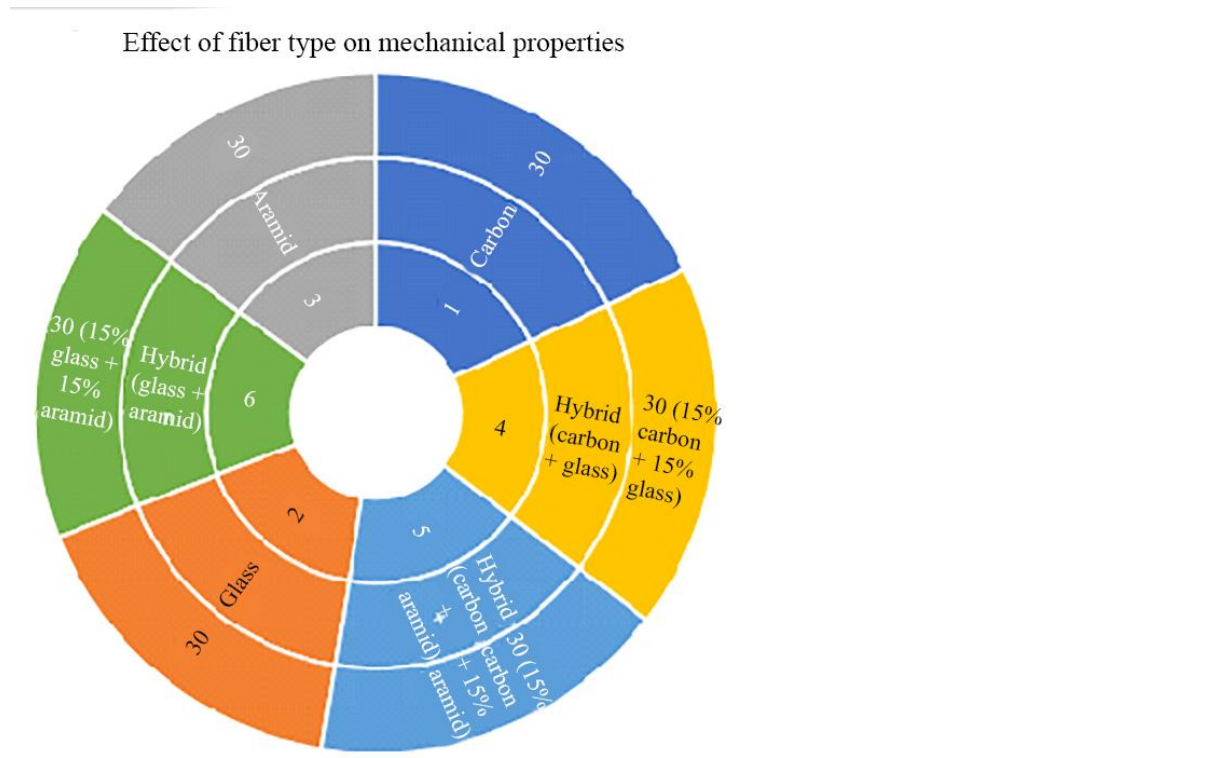


Figure 3. Effect of fiber type and hybrid combinations on tensile strength, compressive strength, and impact strength of epoxy composites as presented in Table 2.

Table 2. Effect of fiber type on mechanical properties.

Fiber type	Fiber volume fraction (%)	Tensile strength (MPa)	Compressive strength (MPa)	Impact strength (J/m)
Carbon	30	850	500	25
Glass	30	780	480	20
Aramid	30	700	460	18
Hybrid (carbon + glass)	30 (15% carbon + 15% glass)	820	490	22
Hybrid (carbon + aramid)	30 (15% carbon + 15% aramid)	810	470	21
Hybrid (glass + aramid)	30 (15% glass + 15% aramid)	760	460	19

This configuration combines the stiffness of carbon fibers with the flexibility of glass fibers, resulting in a well-balanced composite. The impact strength (22 J/m) highlights an improvement over glass fibers, indicating the hybrid’s ability to handle dynamic loads more effectively than individual glass fibers.

Compared to other configurations in Table 2, the glass and aramid fiber hybrid has a somewhat lower compressive strength (460 MPa) and tensile strength (760 MPa). The hybrid of carbon and aramid fibers exhibits superior properties compared to aramid fibers alone, with a tensile strength of 810 MPa and compressive strength of 470 MPa. These results emphasize the role of fiber synergy in enhancing the mechanical performance of the composite. The strategic hybridization of fibers allows the composites to cater to diverse applications, particularly in environments demanding a combination of strength, durability, and energy dissipation.

Figure 4 shows the thermal behavior of several fiber-reinforced epoxy composites, with an emphasis on important variables such as glass transition temperature, thermal conductivity, and thermal expansion coefficient. It showcases the individual and synergistic thermal properties of pure carbon, glass, and aramid fibers, as well as their hybrid combinations. The data underscores the unique contributions of hybrid reinforcements, which combine the characteristics of multiple fibers, enhancing the overall thermal performance of the composite system.

Thermal properties of hybrid fiber-reinforced epoxy composites

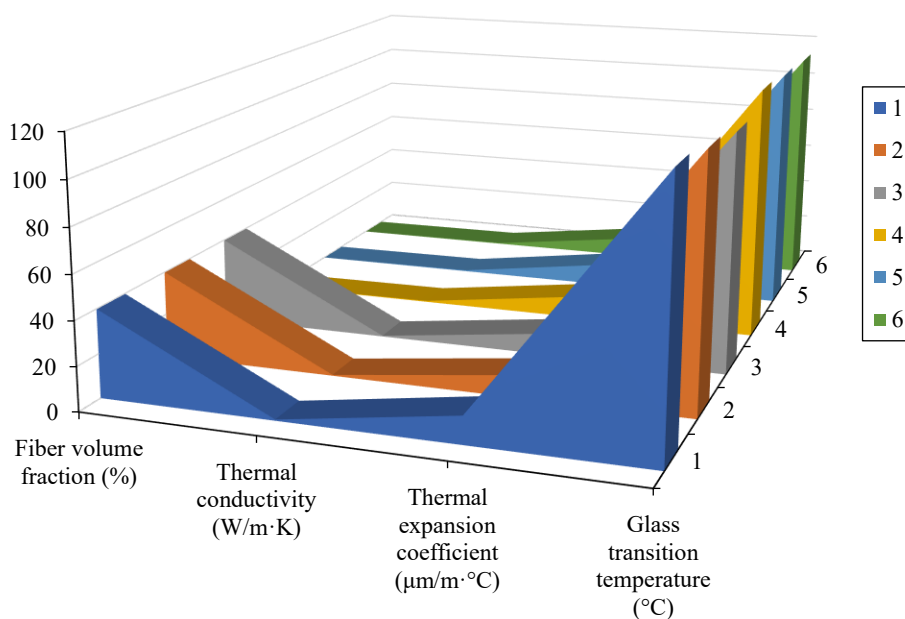


Figure 4. Thermal behavior of carbon, glass, aramid, and hybrid fiber-reinforced composites, including thermal conductivity, thermal expansion coefficient, and glass transition temperature (Table 3).

Table 3. Thermal properties of hybrid fiber-reinforced epoxy composites

Fiber Type	Fiber volume fraction (%)	Thermal conductivity (W/m·K)	Thermal expansion coefficient ($\mu\text{m}/\text{m}\cdot^{\circ}\text{C}$)	Glass transition temperature ($^{\circ}\text{C}$)
Carbon	40	0.55	12.5	120
Glass	40	0.40	9.8	115
Aramid	40	0.35	10.2	110
Hybrid (Carbon + Glass)	40 (20% Carbon + 20% Glass)	0.50	11.0	118
Hybrid (Carbon + Aramid)	40 (20% Carbon + 20% Aramid)	0.48	11.5	115
Hybrid (Glass + Aramid)	40 (20% Glass + 20% Aramid)	0.42	10.5	113

The results indicate that carbon fiber composites exhibit the highest thermal conductivity, attributed to carbon's intrinsic ability to efficiently transfer heat. Thermal expansion coefficient was higher compared to glass, which suggests that while carbon provides excellent heat dissipation, it not effectively resists dimensional changes under temperature variations. Glass fibers, on the other hand, demonstrate lower thermal conductivity but possess the smallest thermal expansion coefficient, indicating better thermal stability. Aramid fibers show intermediate performance, emphasizing their ability to maintain relatively moderate thermal stability and conductivity.

Hybrid composites, such as the combination of carbon and glass fibers, optimize these properties by leveraging the heat dissipation characteristics of carbon with the dimensional stability of glass. This synergy was evident in the reduced thermal expansion coefficient and slightly lowered thermal conductivity compared to pure carbon composites. Similarly, the hybrid of carbon and aramid fibers balances conductivity and expansion, making them suitable for applications requiring moderate thermal resistance and stability. The glass and aramid hybrid offers a unique combination of lower conductivity and moderate thermal expansion, suited for environments where thermal stability was critical.

Table 3 displays since pure carbon composites have the greatest glass transition temperature and perform better at higher temperatures, the trends in glass transition temperature further support the findings. Glass and aramid hybrids present slightly lower values, showing their adaptability for applications with less demanding thermal requirements. These insights collectively highlight how hybrid reinforcements can be tailored to optimize thermal performance, balancing heat transfer, stability, and resilience under cyclic thermal conditions in epoxy-based polymer composites.

The results of the interfacial bonding tests, as illustrated in the provided Figure 5 and Table 4, reveal significant insights into the mechanical performance of various fiber types under different testing conditions. Carbon fiber demonstrates superior interfacial properties compared to glass fiber in both single fiber pull-out and microbond tests. Specifically, carbon fiber exhibits higher maximum pull-out force and interfacial shear strength, highlighting its stronger adhesion with the polymer matrix. This behavior was critical in reinforcing composites where load transfer between the fiber and matrix plays a pivotal role in mechanical stability. The pull-out energy of carbon fiber also surpasses that of glass fiber, further emphasizing its energy absorption capacity during fiber debonding and pull-out.

The hybrid fiber system, combining carbon and glass fibers, showcases enhanced interfacial bonding characteristics compared to individual fibers. The hybrid configuration achieves the highest values in all measured parameters, including maximum pull-out force, interfacial shear strength, and pull-out energy. This improvement was attributed to the synergistic interaction between carbon and glass fibers, where carbon fiber provides superior stiffness and strength, while glass fiber contributes to energy dissipation and flexibility. The combination of these attributes optimizes the stress distribution at the fiber-matrix interface, resulting in improved mechanical performance under cyclic loading.

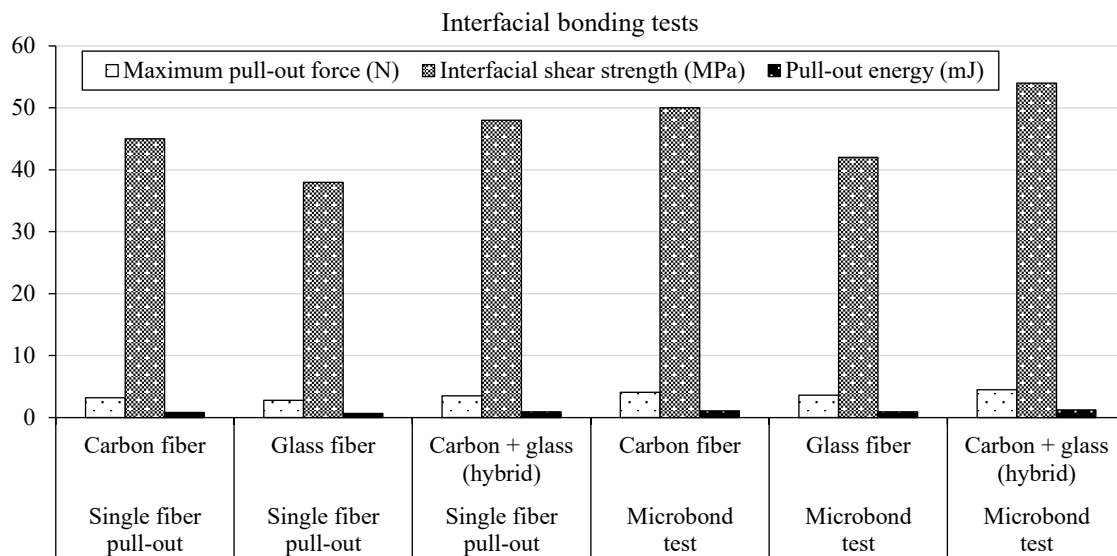


Figure 5. Interfacial bonding behavior from single-fiber pull-out and microbond tests, comparing maximum pull-out force, interfacial shear strength, and pull-out energy for individual and hybrid fibers (Table 4).

Table 4. Results of interfacial bonding tests (single fiber pull-out and microbond tests).

Test type	Fiber type	Maximum pull-out force (N)	Interfacial shear strength (MPa)	Pull-out energy (mJ)
Single fiber pull-out	Carbon fiber	3.2	45	0.85
Single fiber pull-out	Glass fiber	2.8	38	0.65
Single fiber pull-out	Carbon + glass (hybrid)	3.5	48	0.95
Microbond test	Carbon fiber	4.1	50	1.10
Microbond test	Glass fiber	3.6	42	0.92
Microbond test	Carbon + glass (hybrid)	4.5	54	1.25

A notable distinction between the single fiber pull-out and microbond tests was observed in the measured interfacial properties. The microbond test consistently yields higher values for all parameters, indicating its ability to capture the local interfacial shear strength and energy absorption more accurately. This discrepancy can be linked to the differences in test methodologies, with the microbond test focusing on a smaller, localized interfacial area, thereby minimizing the influence of fiber misalignment and matrix heterogeneity. Such insights underscore the importance of test selection in accurately evaluating the interfacial properties of composite materials.

The findings emphasize the critical role of fiber-matrix adhesion in determining the fracture toughness and load-bearing capacity of epoxy-based composites. The superior performance of carbon fiber and the enhanced properties of hybrid fiber systems validate their potential in applications requiring high strength and durability. These results also highlight the significance of optimizing fiber selection and hybridization strategies to achieve tailored mechanical properties for specific engineering applications. The enhanced interfacial bonding properties observed in hybrid configurations could significantly contribute to the long-term reliability and structural integrity of composite materials under demanding cyclic loading conditions.

$$k_{\text{hybrid}} = k_m(1 - \phi) + \sum_{i=1}^n \phi_i k_i \quad (1)$$

Equation 1 models the effective thermal conductivity of hybrid composites by accounting for the thermal properties and volume fractions of the matrix and fibers. It emphasizes the contribution of

each fiber type (carbon, glass, aramid) to overall heat transfer. Variations in fiber volume fractions directly influence thermal management performance.

$$\alpha_{hybrid} = \frac{(1-\phi)\alpha_m E_m + \sum_{i=1}^n \phi_i \alpha_i E_i}{(1-\phi)E_m + \sum_{i=1}^n \phi_i E_i} \quad (2)$$

Equation 2 evaluates the effective thermal expansion of the composite by considering the stiffness and expansion properties of fibers and the matrix. It highlights the ability of hybridization to tailor expansion coefficients, minimizing thermal stresses during temperature changes.

$$\tau = \frac{F}{\pi dl} + \gamma_{hybrid} \quad (3)$$

Equation 3 quantifies the bonding strength at the fiber-matrix interface, critical for load transfer. The additional term γ_{hybrid} captures the synergistic effects of fiber hybridization, enhancing composite performance under mechanical stresses.

$$\sigma_{hybrid} = E_{hybrid} \cdot \epsilon \quad (4)$$

This relationship predicts the stress developed in the composite under strain, where the hybrid elastic modulus combines contributions from the matrix and multiple fiber types. It demonstrates how hybridization enhances stiffness and mechanical strength.

$$G_c = \frac{P^2}{2B\Delta} + \eta_{hybrid} \quad (5)$$

Equation 5 calculates the fracture toughness by combining the energy absorbed at crack tips and the additional toughness provided by hybridization. It shows how hybridization improves resistance to crack growth and damage under cyclic loading.

$$\frac{da}{dN} = C_{hybrid} (\Delta K)^m \quad (6)$$

Equation 6 predicts crack growth per cycle in hybrid composites under fatigue loading. The hybrid material constant (C_{hybrid}) represents the enhanced resistance to crack propagation due to the combined fiber effects, improving durability.

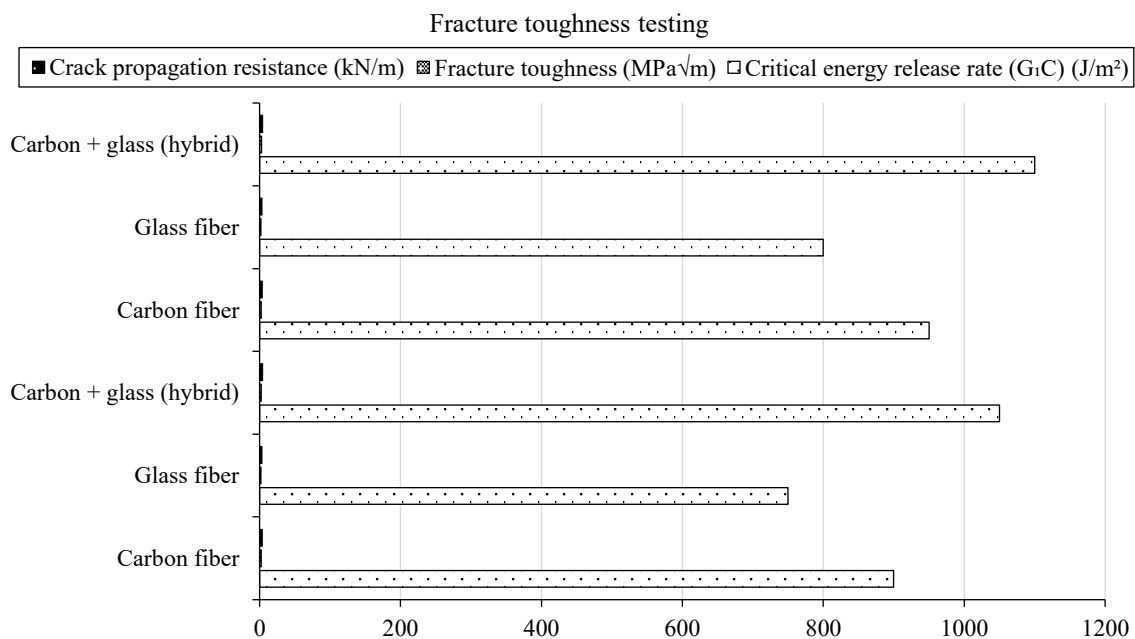


Figure 6. Fracture toughness evaluation using Double Cantilever Beam (DCB) and Compact Tension (CT) tests, showing critical energy release rate, fracture toughness, and crack propagation resistance (Table 5).

Table 5. Results of fracture toughness testing (double cantilever beam and compact tension tests)

Test type	Fiber type	Critical energy release rate (G _{Ic}) (J/m ²)	Fracture toughness (MPa√m)	Crack propagation resistance (kN/m)
Double cantilever beam (DCB)	Carbon fiber	900	2.1	3.5
Double cantilever beam (DCB)	Glass fiber	750	1.8	3.0
Double cantilever beam (DCB)	Carbon + glass (hybrid)	1050	2.5	4.0
Compact tension (CT)	Carbon fiber	950	2.2	3.7
Compact tension (CT)	Glass fiber	800	1.9	3.2
Compact tension (CT)	Carbon + glass (hybrid)	1100	2.6	4.3

The fracture toughness test results in Figure 6 show how important fiber type and hybridization are in improving epoxy-based composites' resistance to crack propagation. Carbon fiber exhibits superior fracture toughness and critical energy release rate compared to glass fiber in both DCB and CT tests. These findings underscore the higher stiffness and energy dissipation capabilities of carbon fiber, which contribute to its ability to delay crack initiation and propagation under applied loads. The crack propagation resistance of carbon fiber was also consistently higher, reflecting its strong interfacial bonding with the matrix and its capacity to transfer stress effectively.

The hybrid fiber configuration, combining carbon and glass fibers, achieves the highest performance across all measured parameters. The critical energy release rate and fracture toughness values of the hybrid system exceed those of individual fibers, indicating a synergistic interaction that optimizes energy absorption and crack arrest mechanisms. The crack propagation resistance of the hybrid system was also the highest, suggesting that the integration of glass fiber into the carbon fiber matrix improves flexibility and distributes stresses more uniformly at the crack tip. This enhancement in fracture properties highlights the potential of hybrid systems in applications where toughness and durability are essential.

A comparison of the DCB and CT test results reveals slight variations in the measured properties, which can be attributed to the different stress states and loading conditions employed in these tests. The CT test consistently shows marginally higher critical energy release rates and fracture toughness values, likely due to the constrained geometry and mode I/II fracture combination, which better simulates real-world crack growth scenarios. These observations emphasize the importance of employing multiple test methods to capture a comprehensive understanding of the fracture behavior of composite materials.

The data further validate the effectiveness of hybridization in improving the fracture resistance of polymer composites. By combining the strengths of carbon and glass fibers, the hybrid system not only enhances energy dissipation and crack resistance but also addresses the limitations of individual fibers, such as brittleness in carbon fibers and lower strength in glass fibers. This optimized performance underlines the suitability of hybrid configurations for demanding applications requiring a balance between strength, toughness, and long-term reliability under cyclic loading conditions. The design of innovative composite materials for structural and high-performance applications can be guided by the insights gleaned from Table 5.

The effects of various fiber types on cyclic loading performance more especially, the number of cycles to failure and fatigue life enhancements under conditions of constant and variable amplitude fatigue are graphically depicted in Figure 7. The hybrid carbon-glass fiber reinforcement consistently outperforms the individual carbon and glass fibers in both testing scenarios. The synergistic impact of mixing glass and carbon fibers was seen in Table 6, where the hybrid's improved fatigue performance results from its improved capacity to disperse stress.

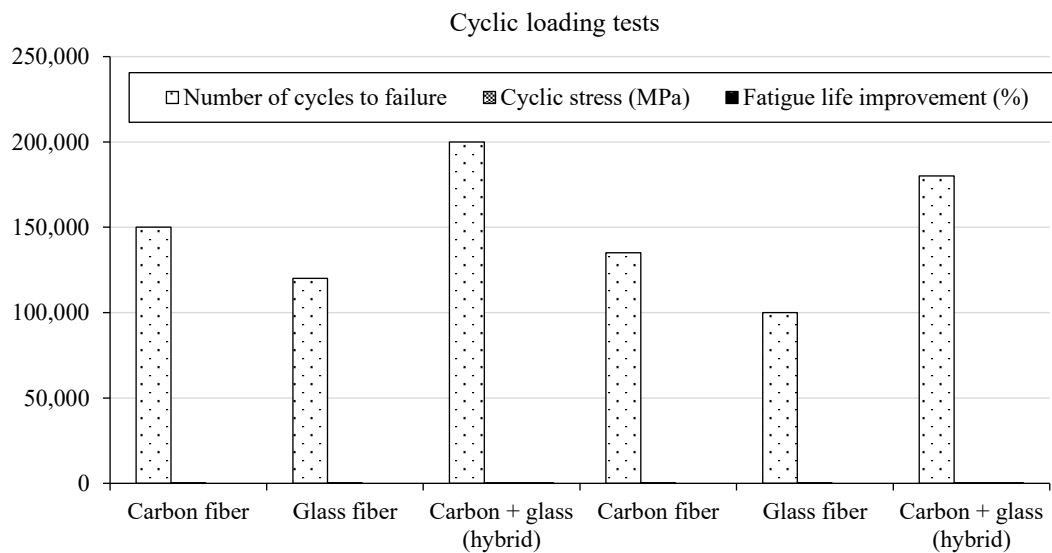


Figure 7. Cyclic loading and fatigue performance of carbon, glass, and hybrid composites under constant and variable amplitude loading, highlighting fatigue life and improvement percentage (Table 6).

Table 6. Results of cyclic loading tests (fatigue testing)

Test parameter	Fiber type	Number of cycles to failure	Cyclic stress (MPa)	Fatigue life improvement (%)
Constant amplitude fatigue	Carbon fiber	150,000	80	-
Constant amplitude fatigue	Glass fiber	120,000	60	-
Constant amplitude fatigue	Carbon + glass (hybrid)	200,000	90	25
Variable amplitude fatigue	Carbon fiber	135,000	75	-
Variable amplitude fatigue	Glass fiber	100,000	55	-
Variable amplitude fatigue	Carbon + glass (hybrid)	180,000	85	30

Carbon fiber, while exhibiting higher fatigue resistance than glass fiber, shows a moderate increase in the number of cycles to failure under both constant and variable amplitude fatigue conditions. This characteristic can be attributed to its intrinsic properties, such as higher tensile strength and stiffness. Glass fiber, on the other hand, exhibits a lower fatigue resistance due to its inherent brittleness and lower modulus of elasticity. It provides cost-effectiveness and acceptable performance in less demanding fatigue conditions.

The hybrid configuration demonstrates a remarkable enhancement in fatigue life, as evident from the increase in the number of cycles to failure and the fatigue life improvement percentages. Under constant amplitude fatigue, the hybrid reinforcement achieves a 25% improvement over the individual fibers, while variable amplitude fatigue sees an even greater improvement of 30%. This indicates that the hybrid reinforcement effectively addresses the limitations of individual fibers, combining the high strength of carbon fiber with the damage tolerance of glass fiber to resist cyclic loading more efficiently.

The ability of the hybrid reinforcement to endure higher cyclic stresses and exhibit longer fatigue life suggests its potential application in high-performance and durability-critical components. The improved interfacial bonding and stress distribution between carbon and glass fibers are likely responsible for these results, reducing the susceptibility to crack initiation and propagation during cyclic loading. This finding underscores the value of hybrid reinforcements in enhancing the mechanical properties and operational reliability of epoxy-based polymer composites.

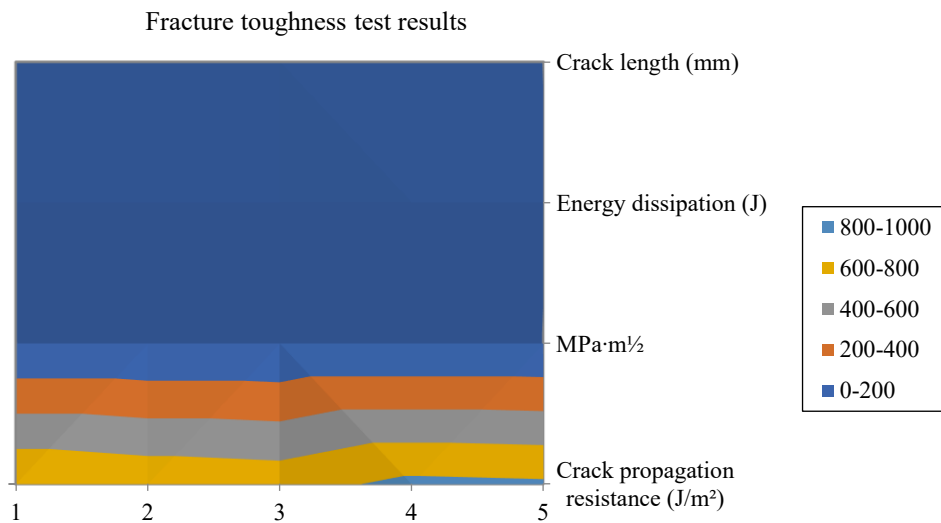


Figure 8. Fracture behavior characteristics, including crack propagation resistance, stress intensity factor (KIC), energy dissipation, and crack length distribution for different composite configurations (Table 7).

Table 7. Fracture toughness test results

Crack propagation resistance (J/m ²)	KIC (MPa·m ^½)	Energy dissipation (J)	Crack length (mm)
800	1.20	10.5	2.1
750	1.15	9.8	2.3
720	1.10	9.2	2.5
850	1.25	11.2	2.0
830	1.22	10.8	2.2

Figure 8 shows the mechanical performance of epoxy-based composites under fracture circumstances, providing important information about their toughness and crack propagation behavior. The crack propagation resistance demonstrates a direct relationship with the interfacial bonding quality and the reinforcement architecture. A peak value of 850 J/m² in crack propagation resistance correlates with the strongest reinforcement, suggesting that effective stress distribution and energy absorption mechanisms in the composite materials contribute to superior resistance to crack growth.

The critical stress intensity factor (KIC) values further reflect the material's ability to withstand fracture initiation under stress. With KIC values ranging from 1.10 to 1.25 MPa·m^½, the observed variations align with the composite's structural response to stress localization at the crack tip. Higher KIC values coincide with improved interfacial bonding, likely facilitated by hybrid fiber reinforcements. This enhancement reduces the likelihood of catastrophic failure, showcasing the material's ability to resist fracture propagation under applied stress.

Energy dissipation values, which range from 9.2 to 11.2 J, indicate the composite's ability to absorb energy before fracture. Higher energy dissipation, observed alongside increased crack propagation resistance, suggests that the composite materials can efficiently distribute the applied energy, delaying crack initiation and propagation. This energy absorption capability, inherent in well-designed hybrid systems, plays a vital role in ensuring the composite's durability and operational safety under demanding conditions.

The results on crack length, which ranges from 2.0 to 2.5 mm, supports the fracture toughness trends seen in Table 7. Shorter crack lengths correspond to higher crack propagation resistance and

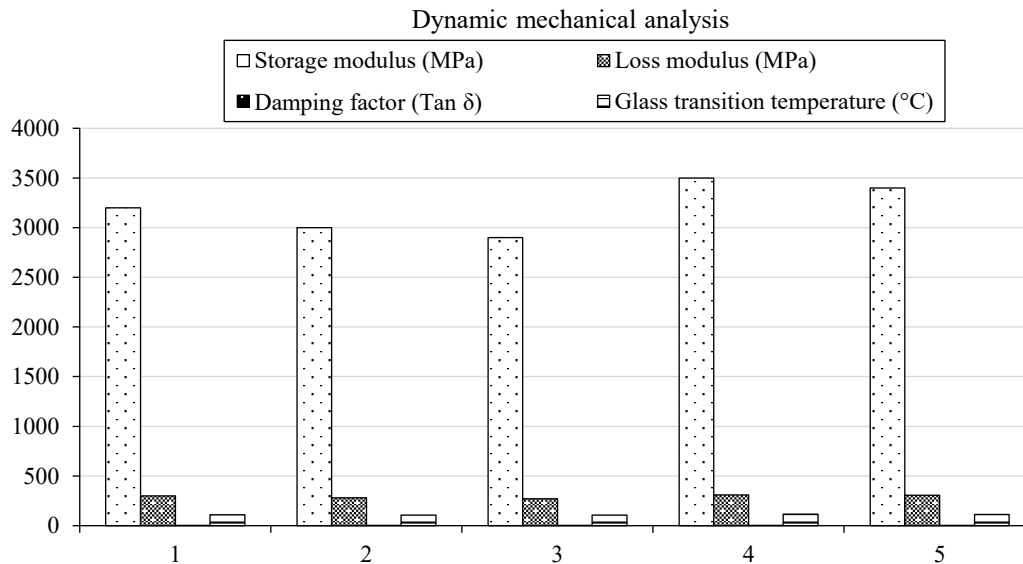


Figure 9. Dynamic mechanical analysis (DMA) results showing storage modulus, loss modulus, damping factor ($\text{Tan } \delta$), and glass transition temperature (T_g) for hybrid and single-fiber composites (Table 8).

Table 8. Dynamic mechanical analysis results.

Storage modulus (MPa)	Loss modulus (Mpa)	Damping factor ($\text{Tan } \delta$)	Glass transition temperature (°C)
3200	300	0.09	110
3000	280	0.10	108
2900	270	0.11	106
3500	310	0.08	115
3400	305	0.09	113

KIC values, emphasizing the effectiveness of the composite structure in resisting crack growth. This outcome underscores the interplay of fiber-matrix bonding, load transfer mechanisms, and the synergistic effects of hybrid reinforcements in tailoring the fracture behavior of polymer composites for enhanced performance under cyclic and impact loading scenarios.

The impact of hybrid fiber reinforcement was highlighted in Figure 9, which shows how the material characteristics change under cyclic stress. The storage modulus values indicate the material's stiffness and elastic behavior. Table 8 shows that samples with a larger storage modulus are better at storing energy when deformed. Across all samples, the storage modulus remains significantly higher than the loss modulus, reinforcing the material's elastic dominance and superior load-bearing capacity. Notably, the highest storage modulus value, 3500 MPa, highlights an optimal reinforcement configuration that maximizes stiffness.

The loss modulus provides insights into the viscous response of the material, indicating energy dissipation as heat. This characteristic plays a crucial role in damping and mechanical stability under repeated stresses. While the loss modulus exhibits slight variations across samples (ranging from 270 to 310 MPa), the consistent trend suggests that hybrid fiber reinforcement achieves a balanced energy dissipation without compromising stiffness. This balance was essential for applications requiring both durability and energy absorption.

The damping factor ($\text{Tan } \delta$) was a critical parameter representing the ratio of energy lost to energy stored during cyclic loading. Values closer to zero signify lower energy loss, aligning with the

material's enhanced performance under dynamic conditions. The damping factor ranges from 0.08 to 0.11, suggesting efficient hybrid reinforcement configurations that reduce internal friction. The lowest damping factor (0.08) correlates with the highest storage modulus, reflecting the synergistic effects of reinforcement on improving both elasticity and resistance to mechanical fatigue.

The glass transition temperature (T_g) marks a pivotal phase transition influencing mechanical properties. Higher T_g values indicate a broader operational temperature range, critical for sustaining performance under thermal fluctuations. The T_g values, ranging from 106°C to 115°C , affirm the effectiveness of hybrid fibers in enhancing the thermal stability of epoxy composites. Samples exhibiting higher T_g (115°C and 113°C) correlate with superior mechanical properties, indicating robust interfacial bonding and reinforcement distribution.

The data collectively underscores the role of hybrid fiber reinforcement in enhancing key mechanical properties such as stiffness, damping, and thermal stability. The interplay of these factors highlights the material's suitability for applications requiring reliability under cyclic stresses, confirming the success of hybrid fiber integration strategies in achieving desirable performance metrics.

Figure 10 shows the interplay between stress amplitude and the material's fatigue performance under cyclic loading conditions. The number of cycles to failure was directly impacted by stress amplitude; in Figure 10, larger stress levels result in faster material deterioration. For example, at 90 MPa, the material exhibits the highest cycles to failure (14,000), showcasing the material's resilience at this threshold. Higher performance was tied to more complex damage mechanisms, indicating a trade-off between durability and structural complexity under increased stress.

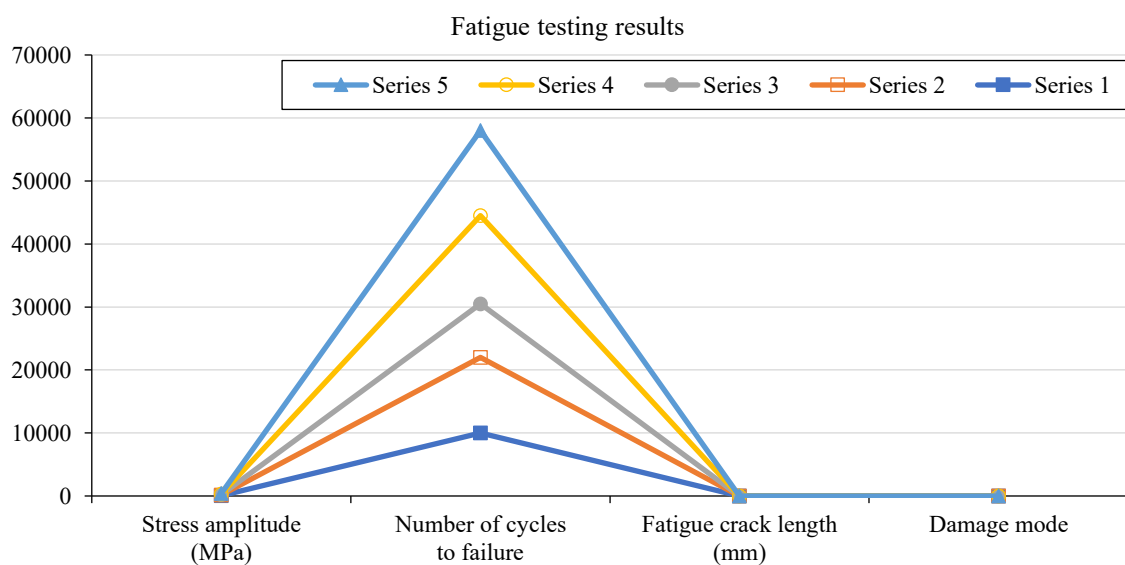


Figure 10. Fatigue testing results showing correlation between stress amplitude, cycles to failure, fatigue crack length, and observed damage mechanisms in epoxy composites (Table 9).

Table 9. Fatigue testing results.

Stress amplitude (MPa)	Number of cycles to failure	Fatigue crack length (mm)	Damage mode
80	10,000	1.5	Matrix cracking
75	12,000	1.3	Fiber debonding
70	8,500	1.8	Delamination
90	14,000	1.2	Combined damage mechanisms
85	13,500	1.4	Crack bridging and pull-out

The number of cycles to failure reflects the material's endurance under repeated loading. Variations in cycle counts across stress amplitudes suggest a correlation between reinforcement efficiency and the resistance to fatigue-induced cracks. The highest recorded cycles (14,000) at 90 MPa stress indicate optimal hybrid fiber reinforcement mechanisms effectively countering fatigue stresses. Conversely, lower cycles at 70 MPa (8,500) signify material susceptibility to earlier crack propagation when subjected to specific configurations or reinforcement distributions.

The progression of fatigue crack length further explains the material's structural response under cyclic stress. Shorter crack lengths correspond to damage mechanisms like fiber debonding or crack bridging, indicating better load transfer and crack arrest capabilities of hybrid reinforcements. For instance, the minimal crack length (1.2 mm) observed at 90 MPa demonstrates effective fiber-matrix interaction, minimizing crack propagation and ensuring structural stability. Table 9 illustrates the lower fiber-matrix adhesion caused by delamination at 70 MPa, which results in larger fracture lengths (1.8 mm).

Damage modes provide insight into the failure mechanisms. Matrix cracking and fiber debonding are primarily observed at lower stress amplitudes, signaling localized failures that do not significantly impact overall integrity. Higher stress levels, combined damage mechanisms and crack bridging dominate, emphasizing the hybrid reinforcement's role in mitigating catastrophic failure. These advanced damage mechanisms distribute the stresses more uniformly, extending the material's life span even under increased loading conditions.

The analysis underscores the effectiveness of hybrid fiber reinforcement in enhancing fatigue resistance through improved crack arrest, reduced propagation, and balanced damage distribution. The material's capability to endure higher stress levels while maintaining structural integrity highlights its suitability for demanding applications requiring prolonged cyclic loading performance. This balance between durability and structural performance was a testament to the robustness of the reinforcement strategies employed.

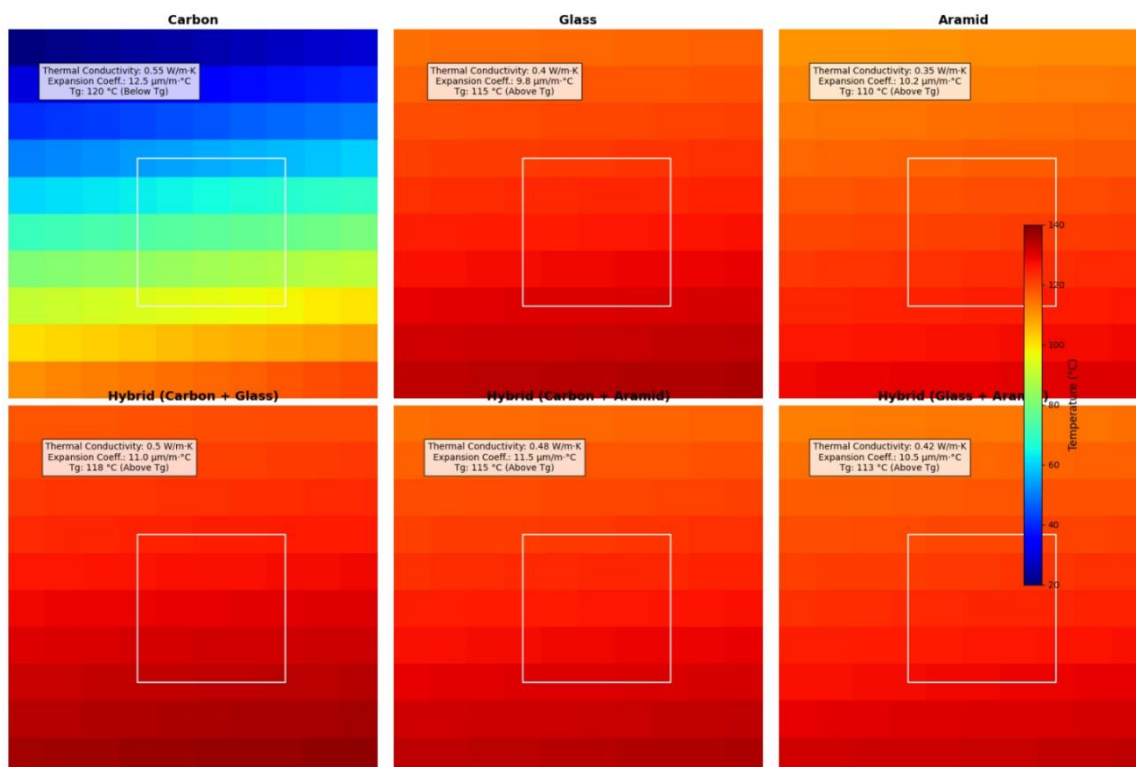


Figure 11. Thermal behavior and material properties of individual and hybrid fiber-reinforced composites

The thermal behavior and properties of various reinforcement materials, both individual and hybrid composites, under thermal conditions. Each subplot provides insight into how different reinforcements, including carbon, glass, aramid, and their hybrids, respond to heat transfer and thermal stress, with significant implications for interfacial bonding, dimensional stability, and mechanical performance.

Figure 11 displays the glass transition temperatures (T_g), expansion coefficients, and thermal conductivity for each material in the top row. Carbon fiber exhibits the highest thermal conductivity ($0.55 \text{ W/m}\cdot\text{K}$) but the largest expansion coefficient ($12.5 \text{ }\mu\text{m/m}\cdot\text{ }^\circ\text{C}$) below its T_g , leading to notable thermal stability at high temperatures. Glass fiber demonstrates moderate thermal conductivity ($0.4 \text{ W/m}\cdot\text{K}$) and a slightly lower expansion coefficient ($9.8 \text{ }\mu\text{m/m}\cdot\text{ }^\circ\text{C}$). T_g was above the operational temperature, indicating stability in high-heat applications. Aramid fiber displays the lowest thermal conductivity ($0.35 \text{ W/m}\cdot\text{K}$) and a reduced expansion coefficient ($10.2 \text{ }\mu\text{m/m}\cdot\text{ }^\circ\text{C}$) but shows high thermal stability above T_g , making it suitable for thermal insulation.

The second row, featuring hybrids, demonstrates improved or balanced thermal properties due to the combination of reinforcements. For instance, the hybrid of carbon and glass fibers shows a thermal conductivity of $0.5 \text{ W/m}\cdot\text{K}$ and a lower expansion coefficient ($11.0 \text{ }\mu\text{m/m}\cdot\text{ }^\circ\text{C}$) above T_g , indicating a trade-off between high conductivity and lower thermal strain. Similarly, the hybrid of carbon and aramid achieves a conductivity of $0.48 \text{ W/m}\cdot\text{K}$ with a reduced expansion coefficient ($11.5 \text{ }\mu\text{m/m}\cdot\text{ }^\circ\text{C}$). The glass and aramid hybrid, while having slightly lower conductivity ($0.42 \text{ W/m}\cdot\text{K}$), offers better stability with an expansion coefficient of $10.5 \text{ }\mu\text{m/m}\cdot\text{ }^\circ\text{C}$, showcasing its suitability in applications requiring dimensional accuracy.

The heatmap patterns highlight how heat was distributed across the materials. In individual fibers, carbon fiber achieves better heat dissipation, indicated by more uniform gradients, while glass and aramid exhibit higher localized thermal concentrations. In hybrids, the thermal distribution becomes more even, reducing hotspots and enhancing heat transfer. This uniformity improves material performance under cyclic loading by mitigating stress concentrations at the interface, a critical aspect of durability in composites.

The findings suggest that hybrid composites effectively optimize thermal and mechanical performance, balancing high conductivity with low expansion rates. The interplay between reinforcement types leads to enhanced interfacial bonding, which plays a pivotal role in resisting delamination and fracture under cyclic thermal and mechanical stresses. These hybrid properties enable their use in advanced structural applications, such as aerospace and automotive industries, where thermal and mechanical reliability was essential.

The synergy achieved by combining different reinforcement fibers, enhancing properties like heat dissipation, expansion control, and stability under high temperatures. This aligns with the broader objective of improving composite performance through hybridization, particularly for applications requiring a balance of thermal conductivity and resistance to thermal strain. The hybrid approach paves the way for designing materials with tailored thermal and mechanical properties, addressing the challenges of fatigue and interfacial bonding in demanding operational environments.

CONCLUSION

This study demonstrates the effectiveness of hybrid fiber reinforcement in enhancing the interfacial bonding, fracture toughness, and overall performance of epoxy-based polymer composites under cyclic loading. By combining the unique properties of carbon, glass, and aramid fibers, hybrid composites achieve a synergistic balance of thermal conductivity, dimensional stability, and mechanical strength. The results highlight the advantages of hybridization, where carbon fibers contribute high thermal conductivity, glass fibers offer structural stability, and aramid fibers provide

excellent energy absorption and crack resistance. Thermal analysis revealed that hybrid composites exhibit improved thermal uniformity and reduced expansion coefficients compared to single-fiber composites, enabling better dimensional stability at elevated temperatures. Mechanical testing further confirmed that the hybrid systems outperform their individual counterparts in resisting delamination and crack propagation, attributed to enhanced stress transfer across fiber-matrix interfaces. SEM analyses validated these findings, showing reduced defects and improved microstructural integrity in the hybrid configurations. Numerical modeling supported the experimental observations, reinforcing the conclusion that hybridization introduces a balance between high conductivity and low thermal strain while maintaining superior mechanical properties. These features make hybrid composites highly suitable for demanding applications in aerospace, automotive, and other advanced sectors requiring lightweight materials with high thermal and mechanical reliability. While hybrid fiber reinforcement significantly improves fatigue life, interfacial bonding, and fracture toughness, it also introduces important trade-offs related to cost and weight. Carbon fibers greatly enhance stiffness and fatigue resistance but substantially increase material cost. Glass fibers are more economical but add weight to the composite and offer lower fatigue performance. Aramid fibers improve energy absorption and cyclic durability but reduce overall stiffness. Therefore, the choice of hybrid configuration must balance these competing factors depending on application demands—whether the priority is maximum fatigue performance, weight reduction, or cost efficiency. Hybrid fiber-reinforced epoxy composites present a promising approach for developing tailored materials with superior performance, addressing key challenges such as interfacial bonding and fatigue resistance. While hybrid fiber systems provide improved fatigue life and fracture toughness, introduce trade-offs related to cost and weight. Carbon fibers, despite their excellent stiffness and thermal conductivity, significantly increase overall material expenses. Aramid fibers enhance energy absorption and fatigue resistance but reduce structural stiffness. Conversely, glass fibers are more economical, though heavier and less fatigue-resistant. Therefore, the choice of hybrid configuration should be guided by application-specific priorities whether the goal was maximum fatigue performance, weight reduction, or cost efficiency. Future work could focus on optimizing fiber orientations and exploring new fiber combinations to further expand the potential of hybrid composites.

REFERENCES

1. Ogbonna, V. E., Popoola, A. P. I., Popoola, O. M., & Adeosun, S. O. (2022). A review on the recent advances on improving the properties of epoxy nanocomposites for thermal, mechanical, and tribological applications: challenges and recommendations. *Polymer-Plastics Technology and Materials*, 61(2), 176-195.
2. Balguri, P. K., Samuel, D. H., & Thumu, U. (2021). A review on mechanical properties of epoxy nanocomposites. *Materials Today: Proceedings*, 44, 346-355.
3. Kumar, S., Samal, S. K., Mohanty, S., & Nayak, S. K. (2018). Recent development of biobased epoxy resins: a review. *Polymer-Plastics Technology and Engineering*, 57(3), 133-155.
4. Rafique, I., Kausar, A., Anwar, Z., & Muhammad, B. (2016). Exploration of epoxy resins, hardening systems, and epoxy/carbon nanotube composite designed for high performance materials: A review. *Polymer-Plastics Technology and Engineering*, 55(3), 312-333.
5. Kausar, A., Rafique, I., Anwar, Z., & Muhammad, B. (2016). Perspectives of epoxy/graphene oxide composite: Significant features and technical applications. *Polymer-Plastics Technology and Engineering*, 55(7), 704-722.
6. Kausar, A., Rafique, I., & Muhammad, B. (2016). Review of applications of polymer/carbon nanotubes and epoxy/CNT composites. *Polymer-Plastics Technology and Engineering*, 55(11), 1167-1191.
7. Yang, G., Park, M., & Park, S. J. (2019). Recent progresses of fabrication and characterization of fibers-reinforced composites: A review. *Composites Communications*, 14, 34-42.
8. Mishra, T., Mandal, P., Rout, A. K., & Sahoo, D. (2022). A state-of-the-art review on potential applications of natural fiber-reinforced polymer composite filled with inorganic nanoparticle. *Composites Part C: Open Access*, 9, 100298.

9. Krishnan, P. (2019). Evaluation and methods of interfacial properties in fiber-reinforced composites. In *Mechanical and Physical Testing of Biocomposites, Fibre-Reinforced Composites and Hybrid Composites* (pp. 343-385). Woodhead Publishing.
10. Liu, J., Xue, Y., Dong, X., Fan, Y., Hao, H., & Wang, X. (2023). Review of the surface treatment process for the adhesive matrix of composite materials. *International Journal of Adhesion and Adhesives*, 126, 103446.
11. Han, N., Zhao, X., & Thakur, V. K. (2023). Adjusting the interfacial adhesion via surface modification to prepare high-performance fibers. *Nano Materials Science*, 5(1), 1-14.
12. Chhetri, S., & Bougherara, H. (2021). A comprehensive review on surface modification of UHMWPE fiber and interfacial properties. *Composites Part A: applied science and manufacturing*, 140, 106146.
13. Swain, S., Muduli, K., Kommula, V. P., & Sahoo, K. K. (2022). Innovations in internet of medical things, artificial intelligence, and readiness of the healthcare sector towards health 4.0 adoption. *International Journal of Social Ecology and Sustainable Development (IJSESD)*, 13(1), 1-14.
14. Farhan, K. Z., Johari, M. A. M., & Demirboğa, R. (2021). Impact of fiber reinforcements on properties of geopolymer composites: A review. *Journal of Building Engineering*, 44, 102628.
15. Yi, B., Xu, Q., & Liu, W. (2022). An overview of substrate stiffness guided cellular response and its applications in tissue regeneration. *Bioactive materials*, 15, 82-102.
16. Swain, S., Oyekola, P. O., & Muduli, K. (2022). Intelligent technologies for excellency in sustainable operational performance in the healthcare sector. *International Journal of Social Ecology and Sustainable Development (IJSESD)*, 13(5), 1-16.
17. Fallahi, H., Kaynan, O., & Asadi, A. (2023). Insights into the effect of fiber–matrix interphase physiochemical-mechanical properties on delamination resistance and fracture toughness of hybrid composites. *Composites Part A: Applied Science and Manufacturing*, 166, 107390.
18. Parmar, H., Khan, T., Tucci, F., Umer, R., & Carlone, P. (2022). Advanced robotics and additive manufacturing of composites: towards a new era in Industry 4.0. *Materials and manufacturing processes*, 37(5), 483-517.
19. Alarifi, I. M. (2024). Revolutionising fabrication advances and applications of 3D printing with composite materials: a review. *Virtual and Physical Prototyping*, 19(1), e2390504.
20. Chandran, M. S., Padmanabhan, K., Dipin Raj, D. K., & Chebiyyam, Y. (2020). A comparative investigation of interfacial adhesion behaviour of polyamide based self-reinforced polymer composites by single fibre and multiple fibre pull-out tests. *Journal of Adhesion Science and Technology*, 34(5), 511-530.
21. Lee, D., Kim, J. H., Lee, S. J., Kim, M., & Kwon, D. J. (2024). Microdroplet pull-out testing: Significance of fiber fracture results. *Polymer Testing*, 141, 108631.
22. Motta de Castro, E., Tabei, A., Cline, D. B., Haque, E., Chambers, L. B., Song, K., ... & Asadi, A. (2025). New insights in understanding the fiber-matrix interface and its reinforcement behavior using single fiber fragmentation data. *Advanced Composites and Hybrid Materials*, 8(1), 1-24.
23. Kaybal, H. B., Ulus, H., Cacik, F., Eskizeybek, V., & Avci, A. (2024). Multi-Scale Mechanical Behavior of Liquid Elium® Based Thermoplastic Matrix Composites Reinforced with Different Fiber Types: Insights from Fiber–Matrix Adhesion Interactions. *Fibers and Polymers*, 25(12), 4935-4950.
24. Alhijazi, M., Zeeshan, Q., Qin, Z., Safaei, B., & Asmael, M. (2020). Finite element analysis of natural fibers composites: A review. *Nanotechnology Reviews*, 9(1), 853-875.
25. Chen, Z., Liu, X., Chen, H., Li, J., Wang, X., & Zhu, J. (2024). Application of epoxy resin in cultural relics protection. *Chinese Chemical Letters*, 35(4), 109194.
26. Xiang, Q., & Xiao, F. (2020). Applications of epoxy materials in pavement engineering. *Construction and Building Materials*, 235, 117529.
27. Mirabedini, A., Ang, A., Nikzad, M., Fox, B., Lau, K. T., & Hameed, N. (2020). Evolving strategies for producing multiscale graphene-enhanced fiber-reinforced polymer composites for smart structural applications. *Advanced Science*, 7(11), 1903501.

28. Hao, Q., Liu, S., Wang, X., Zhang, P., Mao, Z., & Zhang, X. (2024). Progression from graphene and graphene oxide to high-performance epoxy resin-based composite. *Polymer Degradation and Stability*, 110731.
29. Thandavamoorthy, R., Alagarasan, J. K., Mohanavel, V., Velmurugan, P., Al-Otibi, F. O., Hossain, I., ... & Lee, M. (2024). Fabrication of green composite made by Cannabis sativa fiber reinforced granite filler blended epoxy matrix composite–Antimicrobial and structural analysis. *Journal of Materials Research and Technology*, 32, 2474-2481.
30. Malekinejad, H., Carbas, R. J., Akhavan-Safar, A., Marques, E. A., Castro Sousa, F., & da Silva, L. F. (2023). Enhancing fatigue life and strength of adhesively bonded composite joints: A comprehensive review. *Materials*, 16(19), 6468.
31. Liu, T., Liu, X., & Feng, P. (2020). A comprehensive review on mechanical properties of pultruded FRP composites subjected to long-term environmental effects. *Composites Part B: Engineering*, 191, 107958.
32. Jesson, D. A., & Watts, J. F. (2012). The interface and interphase in polymer matrix composites: effect on mechanical properties and methods for identification. *Polymer Reviews*, 52(3), 321-354.
33. Hussain, S. M., Shah, S. Z. H., Megat-Yusoff, P. S. M., & Hussain, M. Z. (2023). Degradation and mechanical performance of fibre-reinforced polymer composites under marine environments:–A review of recent advancements. *Polymer Degradation and Stability*, 110452.
34. Arrabiyeh, P. A., May, D., Eckrich, M., & Dlugaj, A. M. (2021). An overview on current manufacturing technologies: Processing continuous rovings impregnated with thermoset resin. *Polymer Composites*, 42(11), 5630-5655.
35. Boztepe, S., Šimáček, P., Labastie, K., Chevalier, M., Sandre, P., Des, J. M., & Advani, S. G. (2022). Effect of the initial resin distribution in partially impregnated thermoplastic prepregs on consolidation. *Composites Science and Technology*, 225, 109488.
36. Huang, Y., Sun, J., Liu, Y., Li, J., & Zhang, X. (2023). Multiphysics coupling study on impregnation process of hot-melt resin in fiber fabrics for composite material production. *Journal of Thermal Science*, 32(1), 206-222.
37. Memon, G. M., Memon, S. I., Wang, X., Kumar, S., & He, Y. (2025). Impact of mold temperature and fiber velocity on impregnation in carbon fiber polyamide 66 composites. *Physics of Fluids*, 37(1).
38. Hu, W., Centea, T., & Nutt, S. (2020). Effects of material and process parameters on void evolution in unidirectional prepreg during vacuum bag-only cure. *Journal of Composite Materials*, 54(5), 633-645.
39. Nurazzi, N. M., Norrrahim, M. N. F., Sabaruddin, F. A., Shazleen, S. S., Ilyas, R. A., Lee, S. H., ... & Nor, N. M. (2022). Mechanical performance evaluation of bamboo fibre reinforced polymer composites and its applications: a review. *Functional Composites and Structures*, 4(1), 015009.
40. Parameswaranpillai, J., Pulikkalparambil, H., Rangappa, S. M., & Siengchin, S. (2021). *Epoxy Composites*. Wiley: Hoboken, NJ, USA.
41. Sumesh, K. R., Palanisamy, S., Khan, T., Ajithram, A., & Ahmed, O. S. (2024). Mechanical, morphological and wear resistance of natural fiber/glass fiber-based polymer composites. *BioResources*, 19(2), 3271-3289.
42. Palanisamy, S., Kalimuthu, M., Palaniappan, M., Alavudeen, A., Rajini, N., Santulli, C., ... & Al-Lohedan, H. (2022). Characterization of acacia caesia bark fibers (ACBFs). *Journal of Natural Fibers*, 19(15), 10241-10252.
43. Almeshaal, M., Palanisamy, S., Murugesan, T. M., Palaniappan, M., & Santulli, C. (2022). Physico-chemical characterization of Grewia Monticola Sond (GMS) fibers for prospective application in biocomposites. *Journal of Natural Fibers*, 19(17), 15276-15290.
44. Palaniappan, M., Palanisamy, S., Murugesan, T. M., Alrasheedi, N. H., Ataya, S., Tadepalli, S., & Elfar, A. A. (2025). Novel Ficus retusa L. aerial root fiber: a sustainable alternative for synthetic fibres in polymer composites reinforcement. *Biomass Conversion and Biorefinery*, 15(5), 7585-7601.

-
45. Palanisamy, S., Kalimuthu, M., Santulli, C., Palaniappan, M., Nagarajan, R., & Fragassa, C. (2023). Tailoring epoxy composites with *Acacia caesia* bark fibers: Evaluating the effects of fiber amount and length on material characteristics. *Fibers*, 11(7), 63.
 46. Palanisamy, S., Keerthiveetil Ramakrishnan, S., Santulli, C., Khan, T., & Ahmed, O. S. (2024). Mechanical and wear performance evaluation of natural fiber/epoxy matrix composites. *BioResources*, 19(4), 845.
 47. Palanisamy, S., Kalimuthu, M., Azeez, A., Palaniappan, M., Dharmalingam, S., Nagarajan, R., & Santulli, C. (2022). Wear properties and post-moisture absorption mechanical behavior of kenaf/banana-fiber-reinforced epoxy composites. *Fibers*, 10(4), 32.